

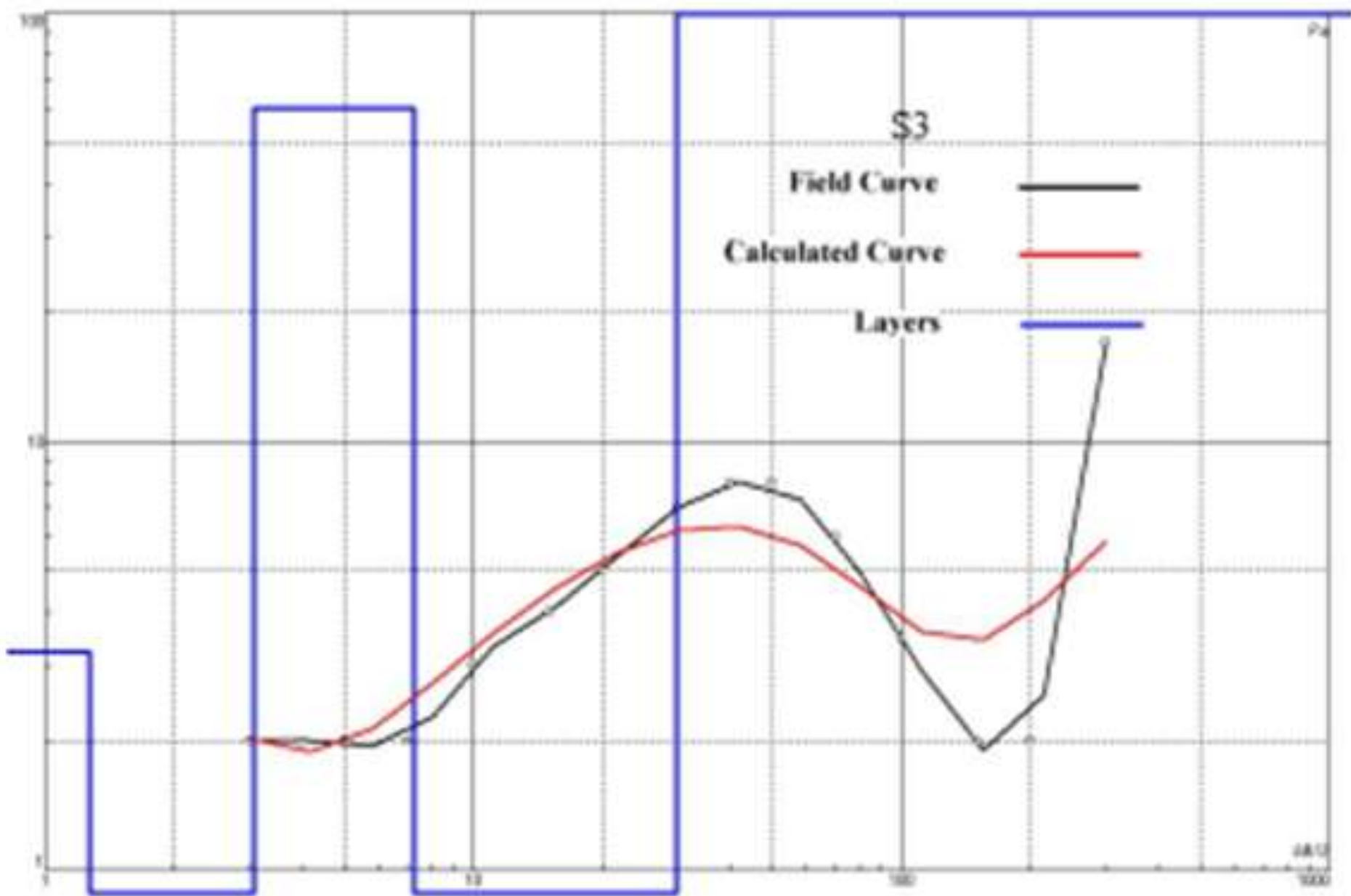


NORAD supported project in MRRD covering
Capacity Building and Institutional Cooperation in the
field of Hydrogeology for Faryab Province
Afghanistan

Geophysics Course

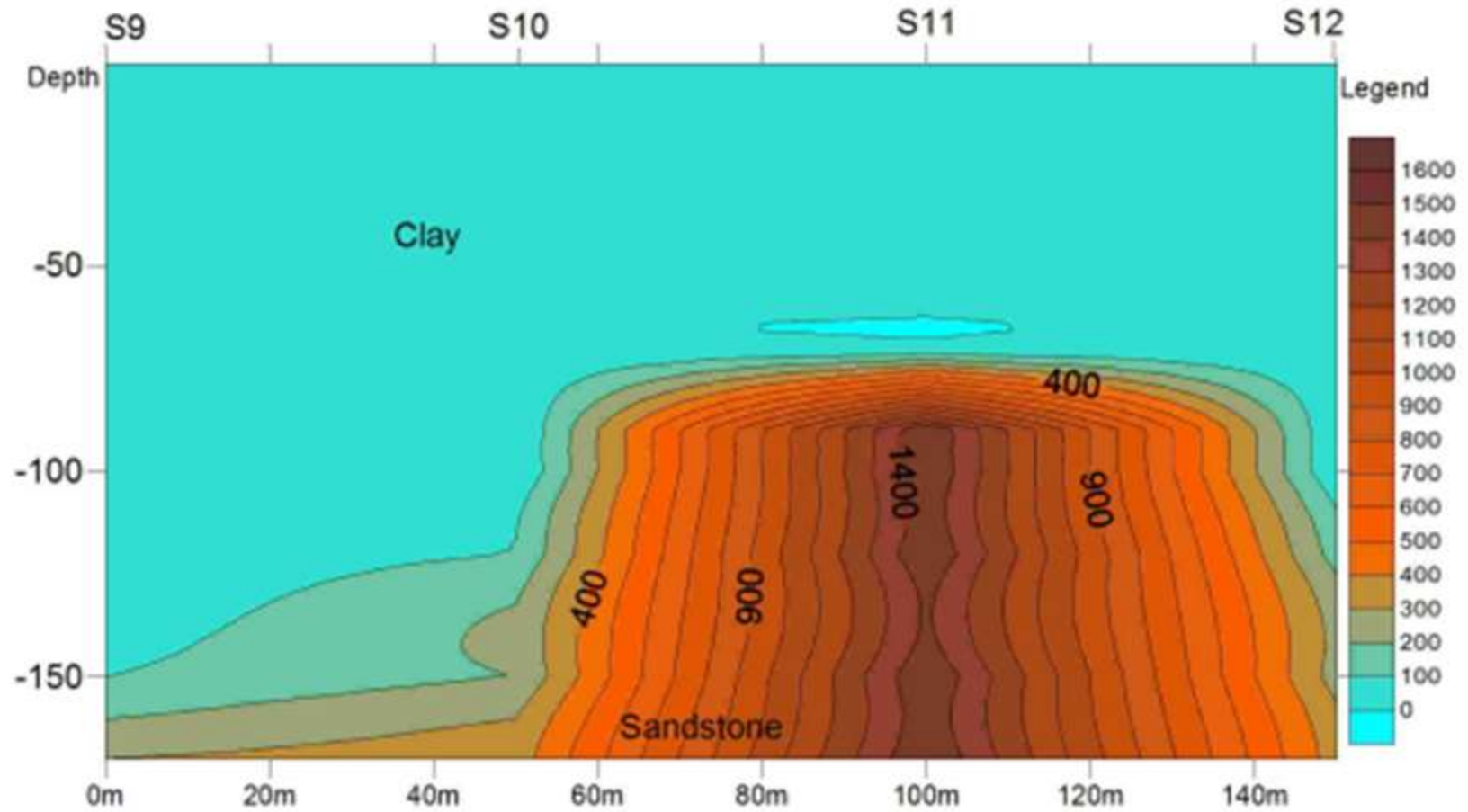
Interpreting DC Resistivity Data

By Andreas de Jong
June 2013



Curve 3. Showing the Apparent Resistivity Curve of Sounding 1.

Geological Cross Section of Profile. 3



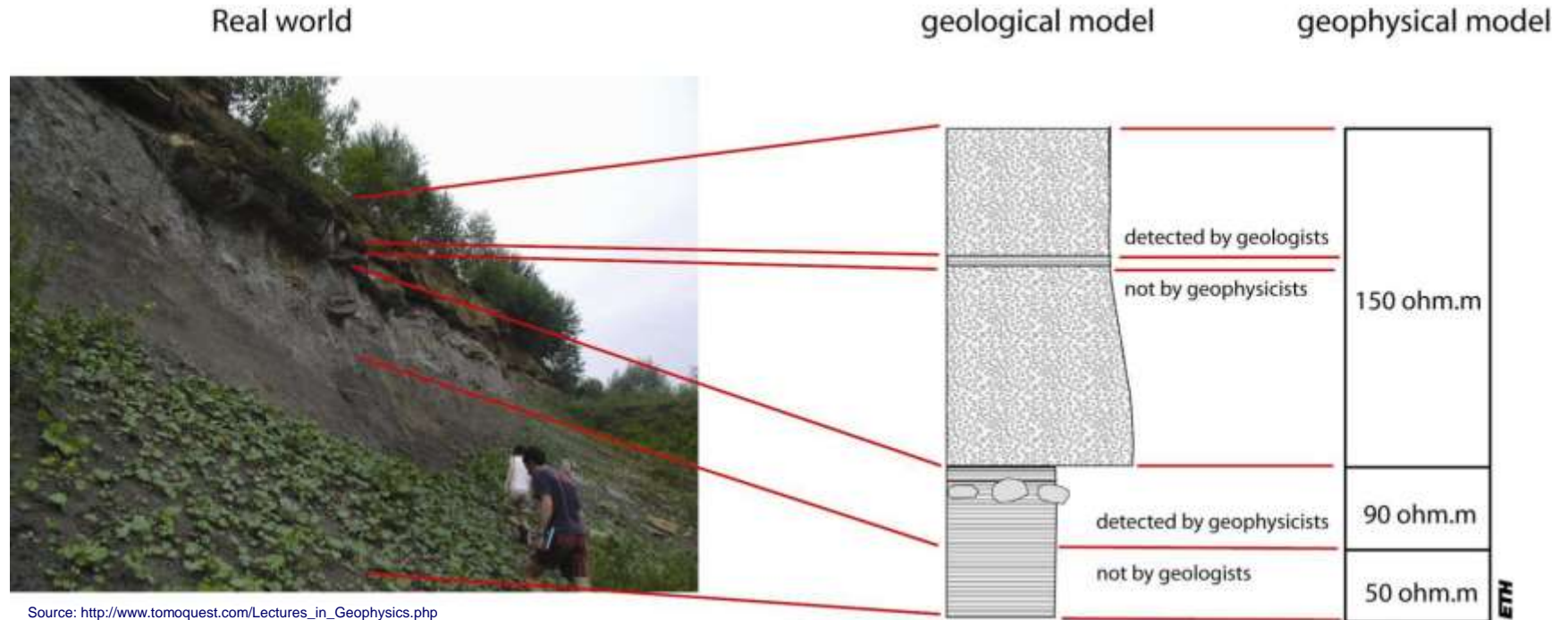
TOPICS TO BE COVERED

1. Introduction
2. Current Flow in the Ground
3. DC Resistivity Surveys
4. VES Interpretation

PART 1 – Introduction

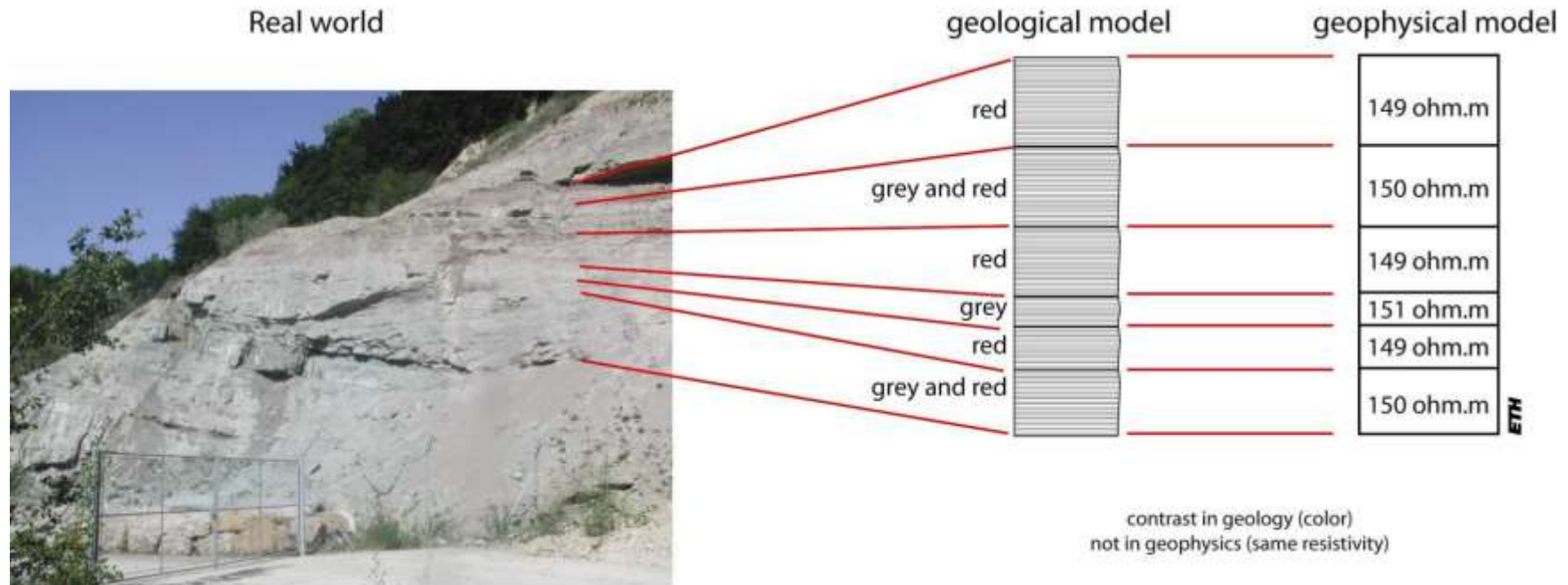
1. Definition of a Model
2. Definition of Contrast
3. Definition of Anomaly
4. Sources of Noise
5. DC Resistivity Sounding Principle & Actual Current Distribution

Definition of a Model



A model is a simple, ideal interpretation of the real world.

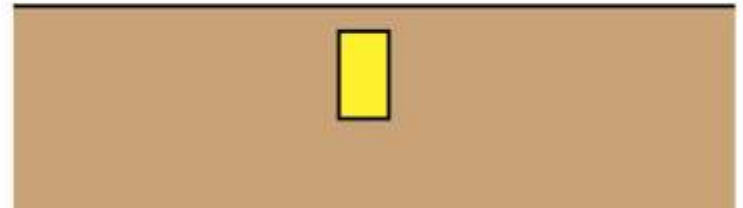
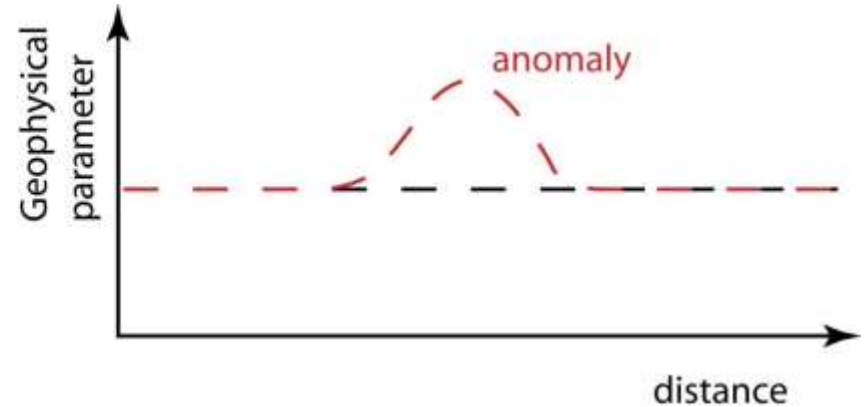
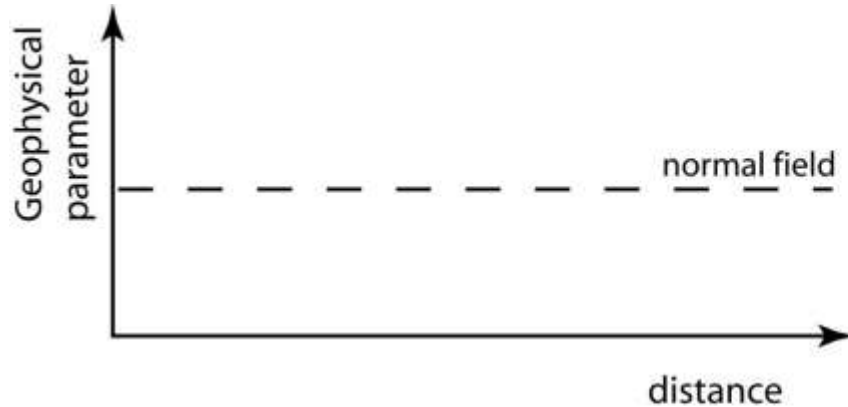
Definition of Contrast



Source: http://www.tomoquest.com/Lectures_in_Geophysics.php

To characterize different material using geophysics, there must be a contrast between the materials (i.e. a difference in the physical properties).

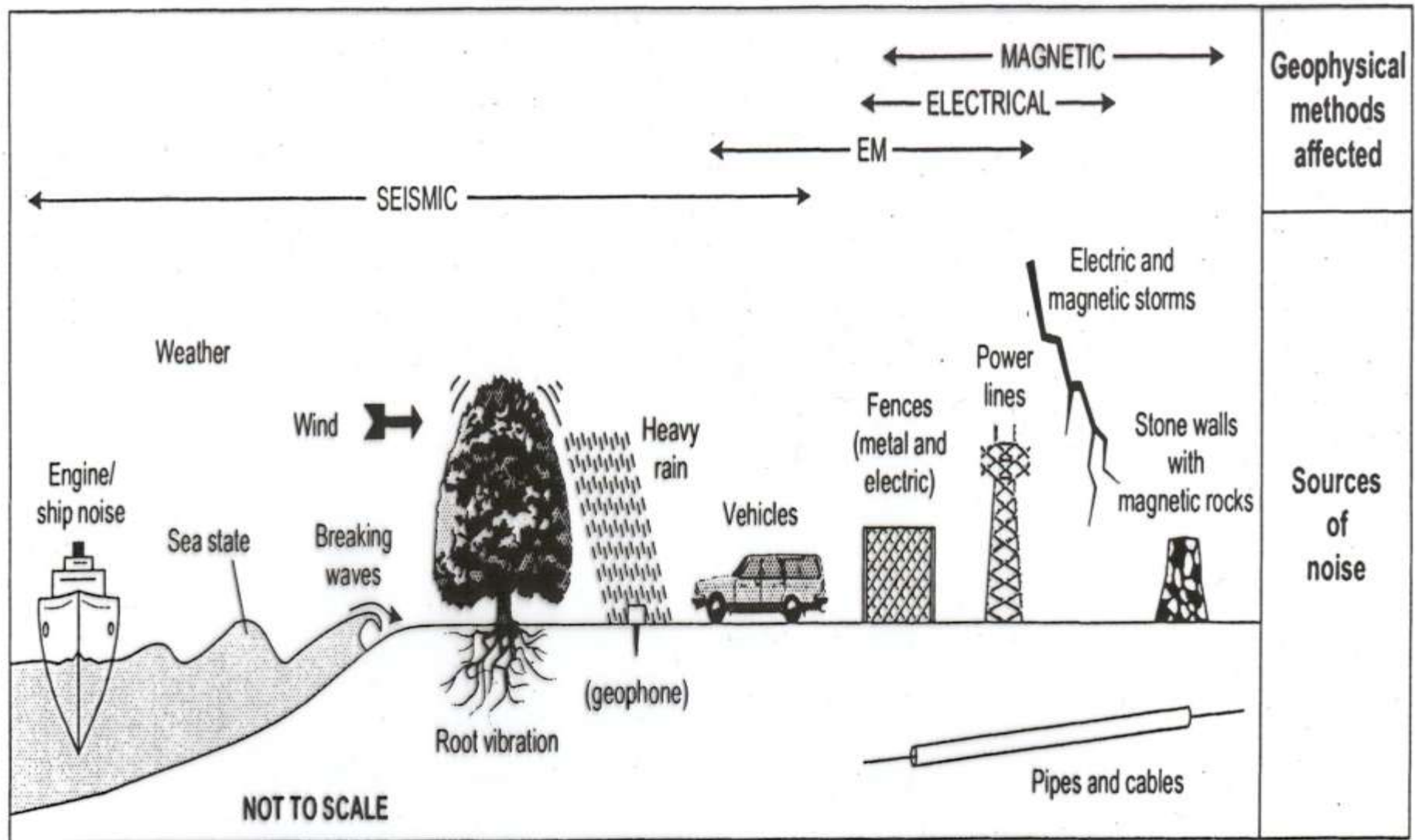
Definition of Anomaly



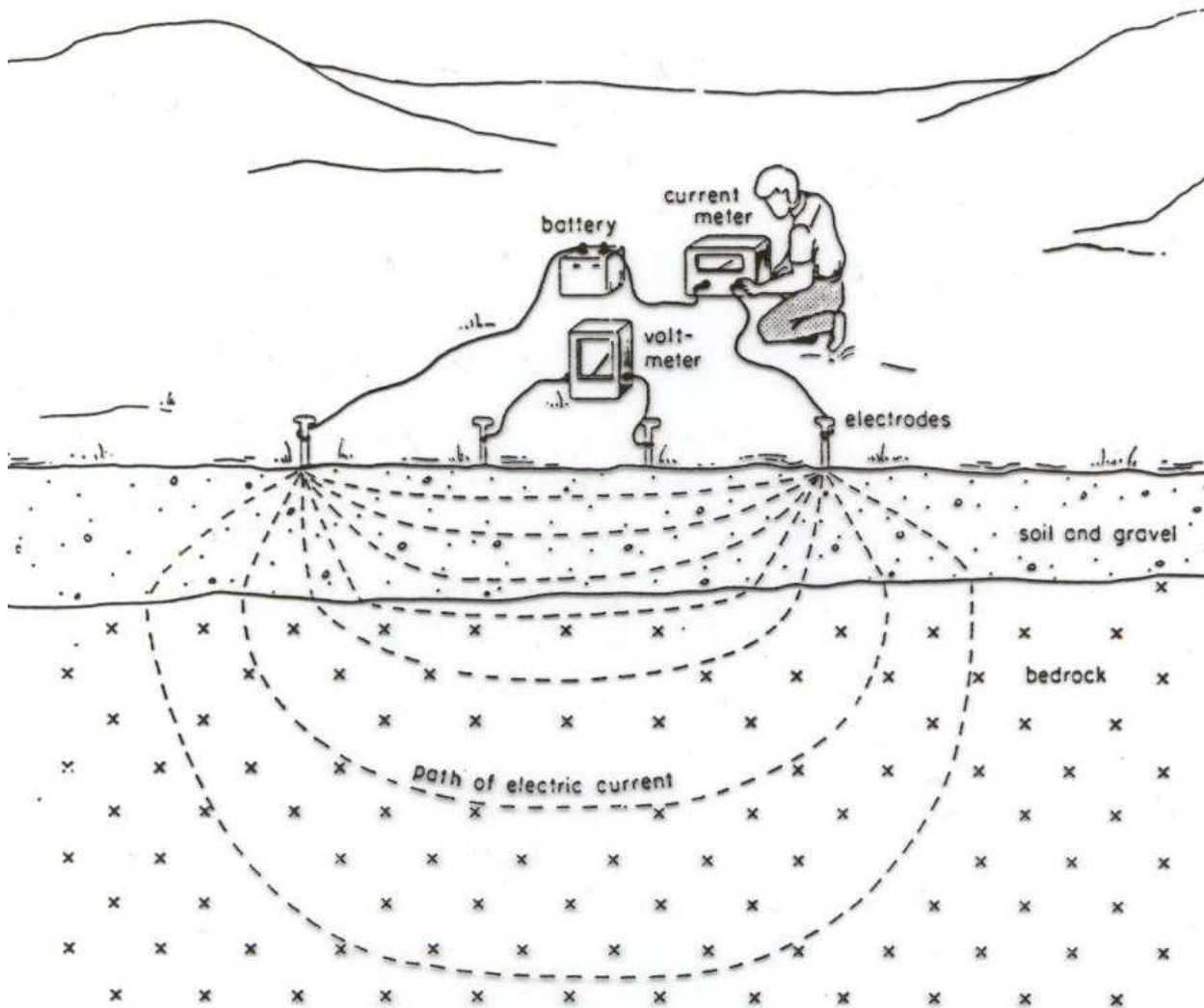
Source: http://www.tomoquest.com/Lectures_in_Geophysics.php

An anomaly is something that deviates from what is standard, normal, or expected.

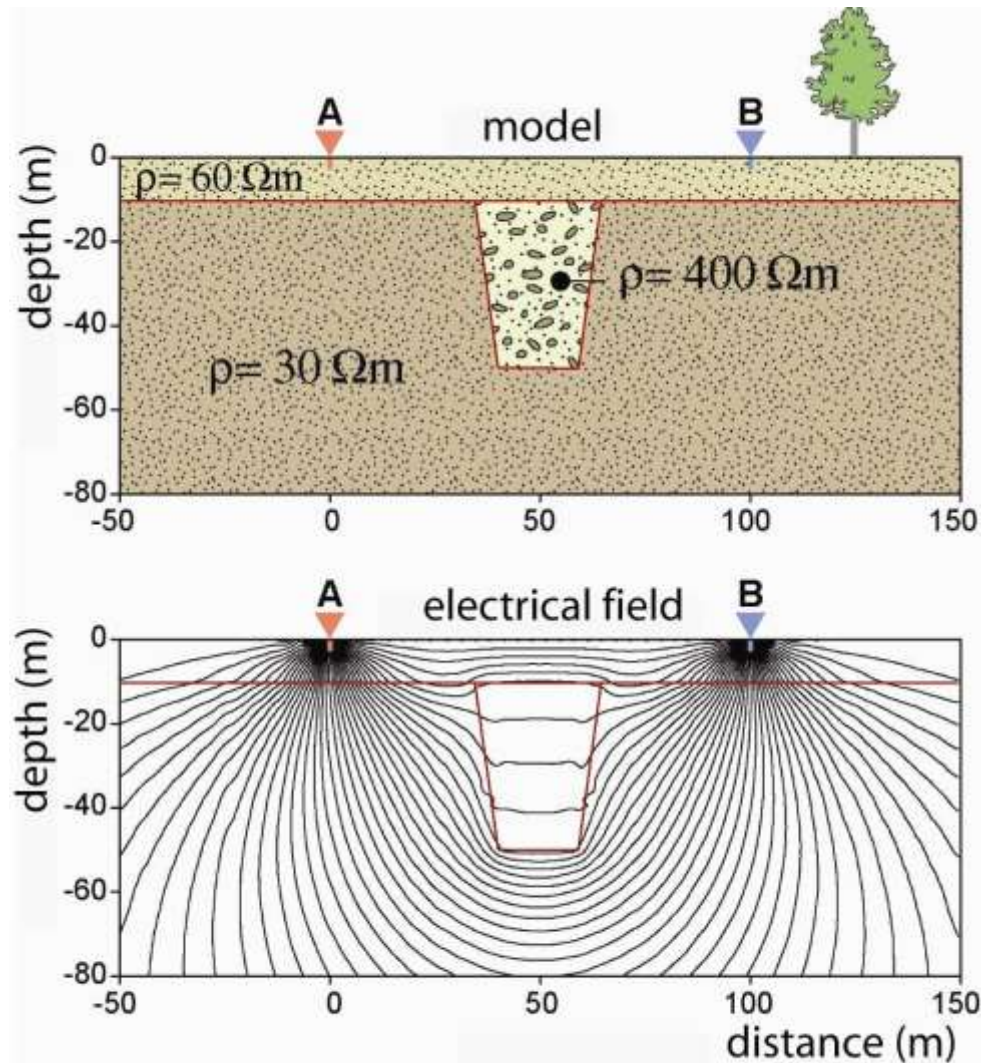
Sources of Noise



DC Resistivity Sounding Principle



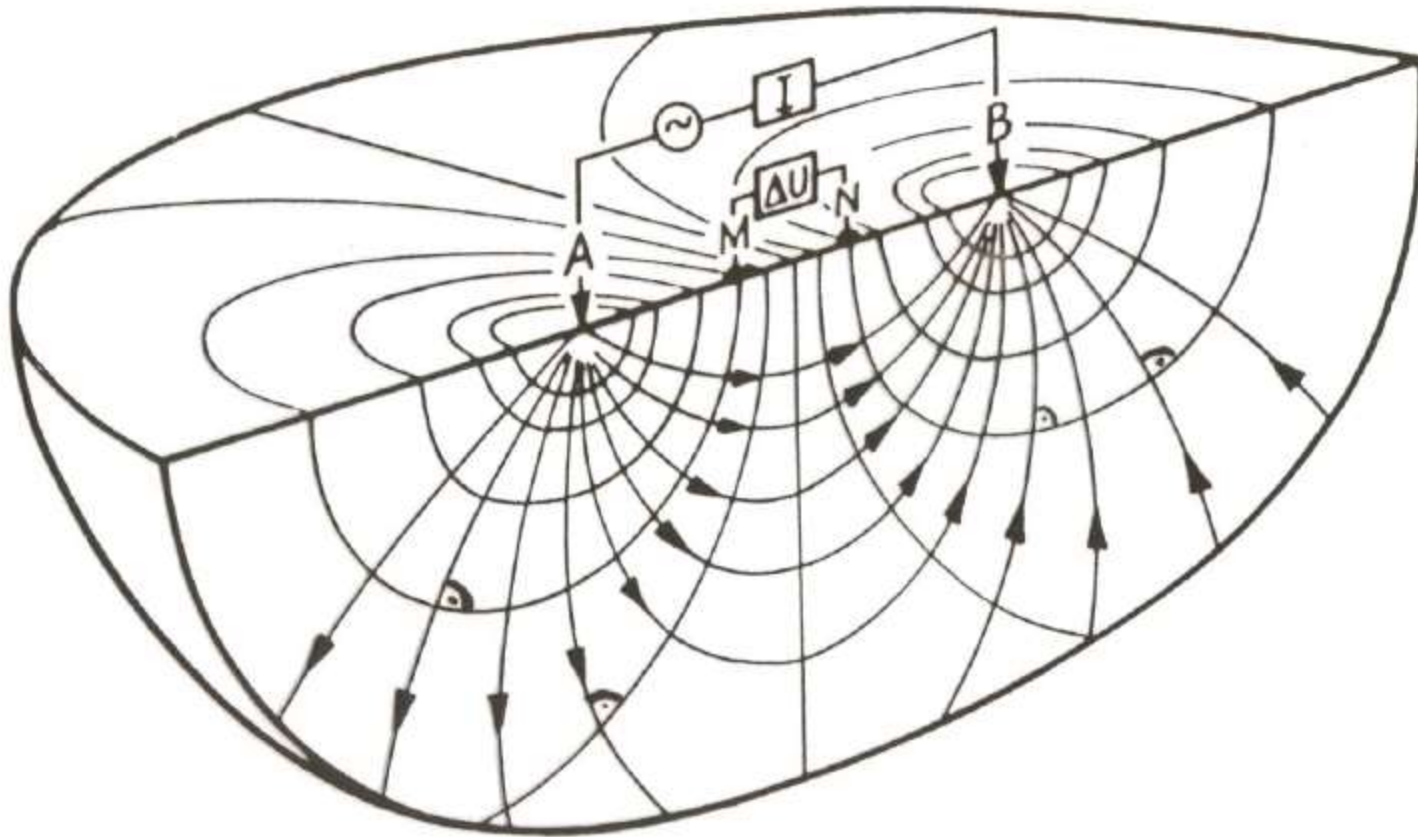
Actual Current Distribution



PART 2 – Current Flow in the Ground (I)

1. Calculating Apparent Resistivity
2. Geometric Factors
3. Equations for Various Arrays
4. Current Penetration
5. Depths of Investigation
6. Effect of A-B Distances on Profiling

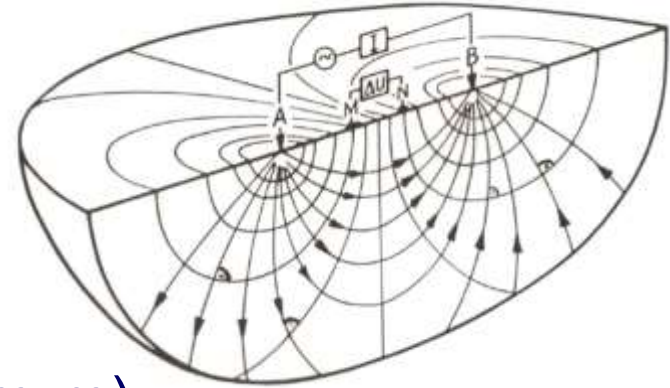
DC Resistivity Sounding



Calculating Apparent Resistivity

Measured resistivity is an apparent resistivity.

$$\rho_a = \frac{\Delta V_{MN}}{I} K$$



ρ_a apparent resistivity (ohm-m)

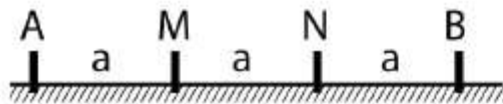
ΔV_{MN} potential (volts) between M and N

I current (amps)

K geometric factor

Geometric Factors of Various Arrays

Wenner



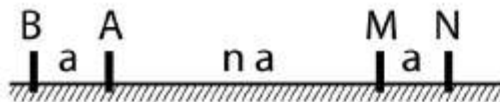
$$K = 2 \pi a$$

Wenner-Schlumberger



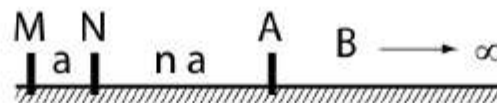
$$K = \pi n (n+1) a$$

dipole-dipole



$$K = \pi n (n+1) (n+2) a$$

pole-dipole



$$K = 2 \pi n (n+1) a$$

pole-pole



$$K = 2 \pi a$$

Equations for Various Arrays

$$\rho_a = 2\pi a \frac{\Delta V}{I}$$

Wenner array

$$\rho_a = \pi n(n+1)a \frac{\Delta V}{I}$$

Schlumberger array

$$\rho_a = \pi n(n+1)(n+2)a \frac{\Delta V}{I}$$

dipole-dipole array

DC Resistivity Field Sheets - Schlumberger



SCHLUMBERGER ARRAY FIELD SHEET

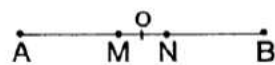
NORPLAN 

Project: _____ Sounding No.: _____

Location: _____ Coordinates East: _____

Equipment: _____ Coordinates North: _____

Operator: _____ Azimuth: _____



$$K = \frac{AM \cdot AN}{MN} \pi$$

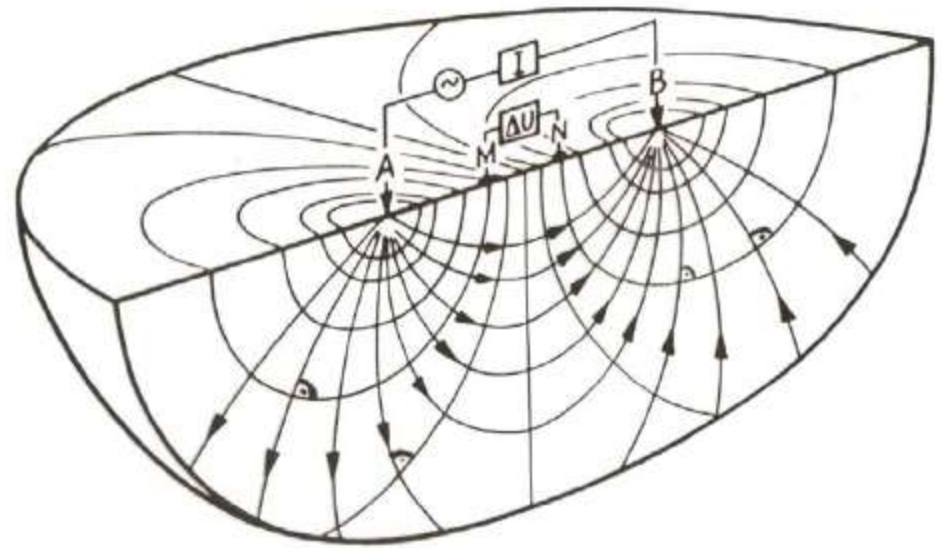
$$\rho_a = K \frac{\Delta V}{I}$$

Marks	OA in m	K for				ΔV in millivolts (mV)	I in milliamperes (mA)	ρ_a in ohm-m (Ωm)
		M N 1m	M N 10m	M N 60m	M N 200m			
1	1	2.35						
2	2	11.8						
3	3	27.5						
1	4	49.5						
2	5	77.7						

NORPLAN 

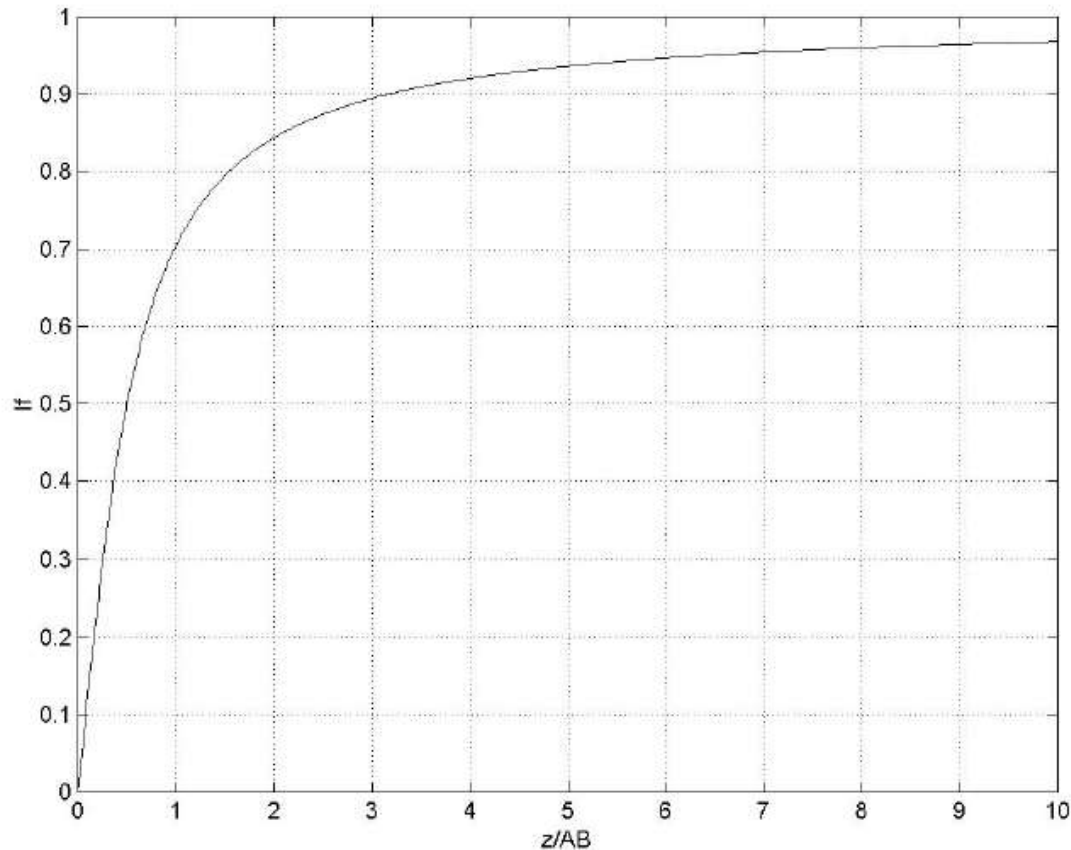
Current Penetration

$$I_f = \left(\frac{2}{\pi} \right) \tan^{-1} \left(\frac{2z}{AB} \right)$$




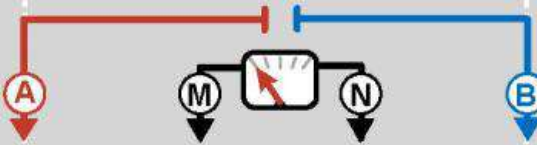
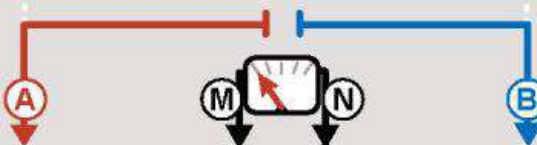


- z depth
- AB distance between current electrodes
- I_f fraction of current penetrating between the surface and z

Current Penetration

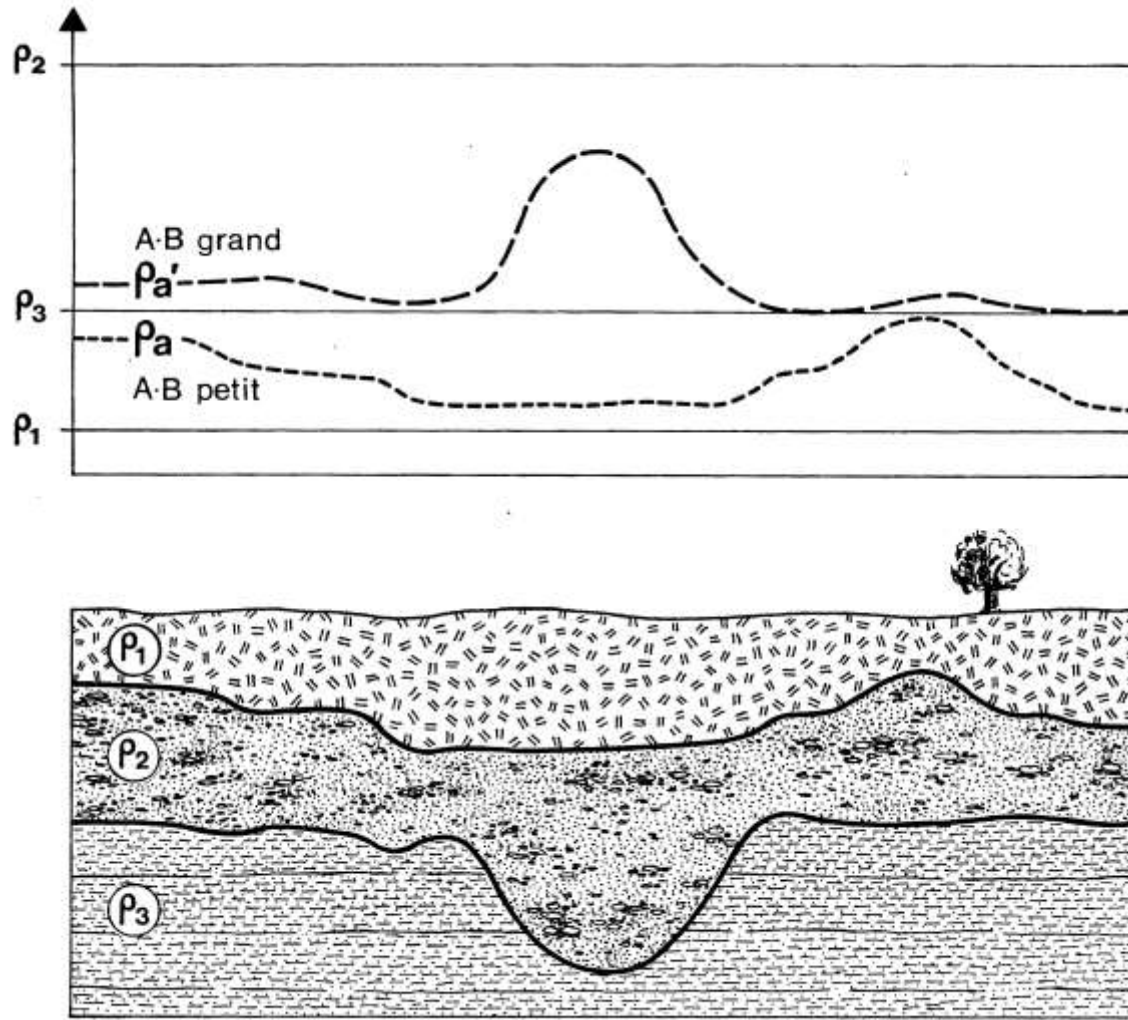


$$I_f = \left(\frac{2}{\pi} \right) \tan^{-1} \left(\frac{2z}{AB} \right)$$

Depths of Investigation

Array		Depth of investigation		Resolving power
		Roy (1971)	Barker (1989)	
Wenner		0.11L	0.17L	1/2.25
Schlumberger		0.125L	0.19L	1/2.45
Dipôle-Dipôle		0.195L	0.25L	1/3.45
Pôle-Pôle		0.35L		1/8.4

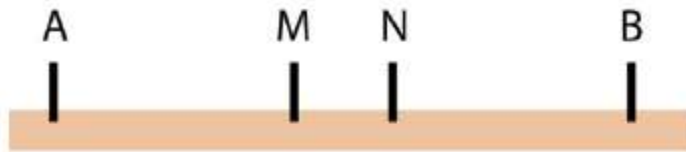
Profiling: Effect of A-B Distances



PART 2 – Current Flow in the Ground (II)

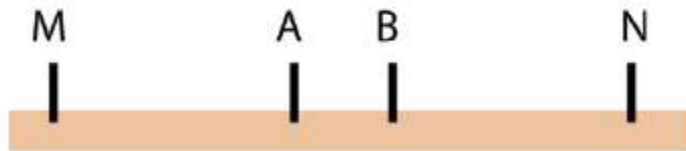
1. Principle of Reciprocity
2. Effects of Heterogeneous Earth
3. Current Flow Lines
4. Effect of Near-Surface Resistivity
5. Effects of Topography
6. Contact Resistance
7. Coping with Noise

Principle of Reciprocity



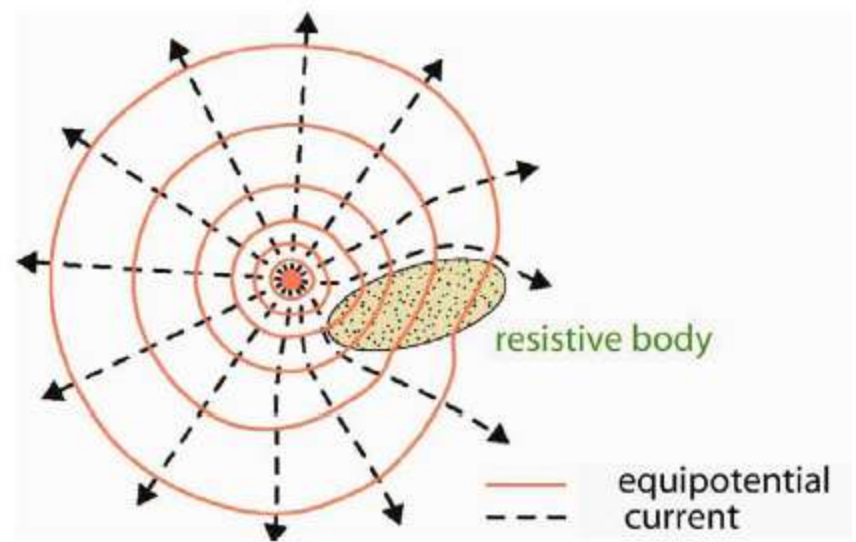
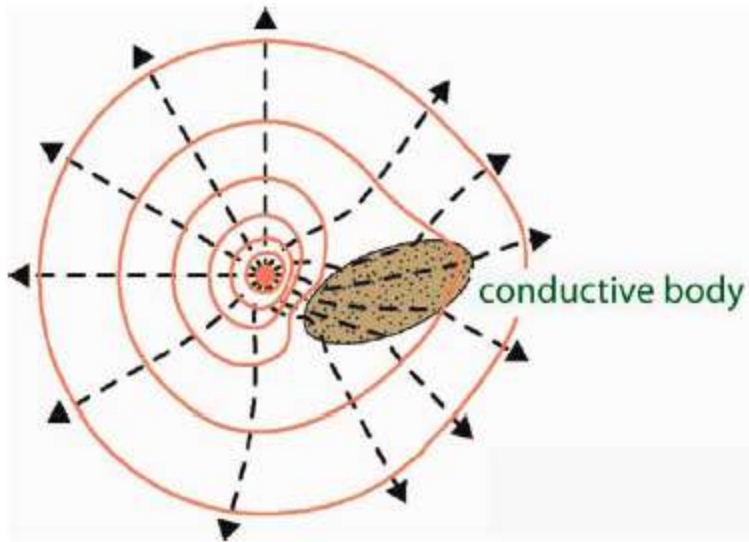
dV_1

$$dV_1 = dV_2$$

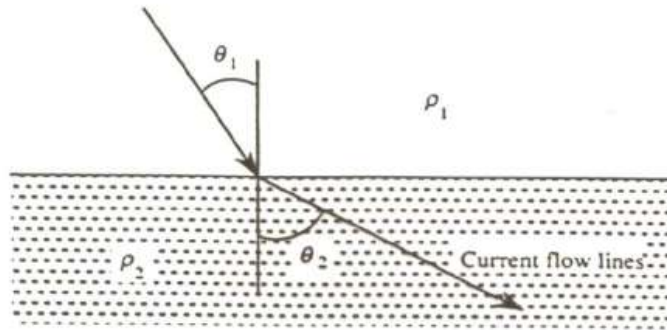


dV_2

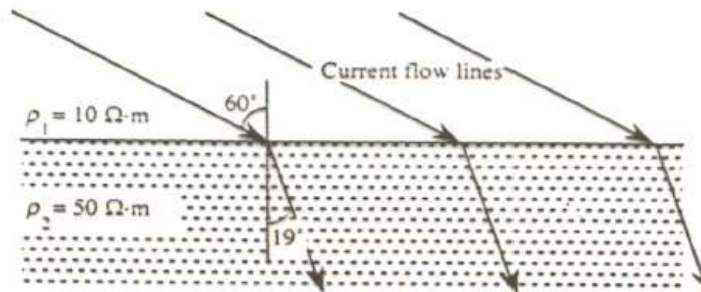
Effects of Heterogeneous Earth



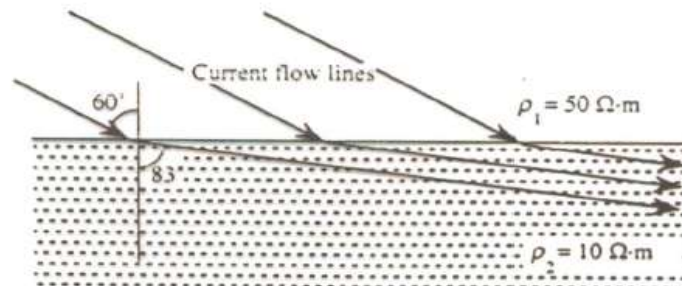
Current Flow Lines



$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\rho_2}{\rho_1}$$

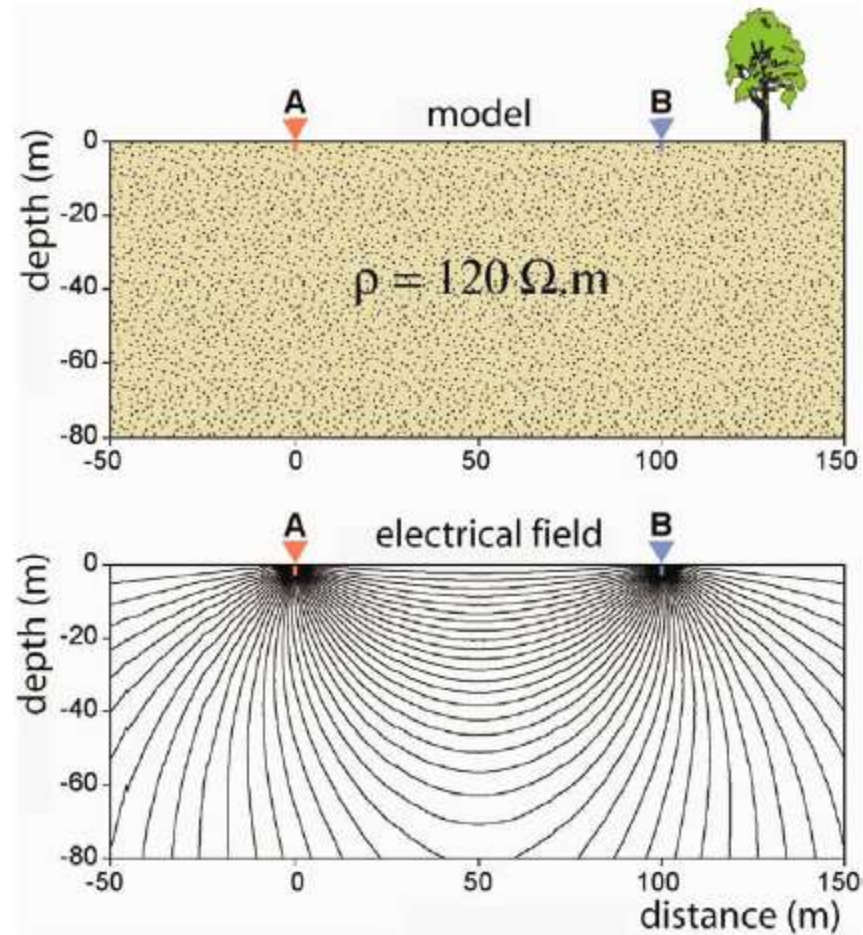


$$\rho_1 < \rho_2$$

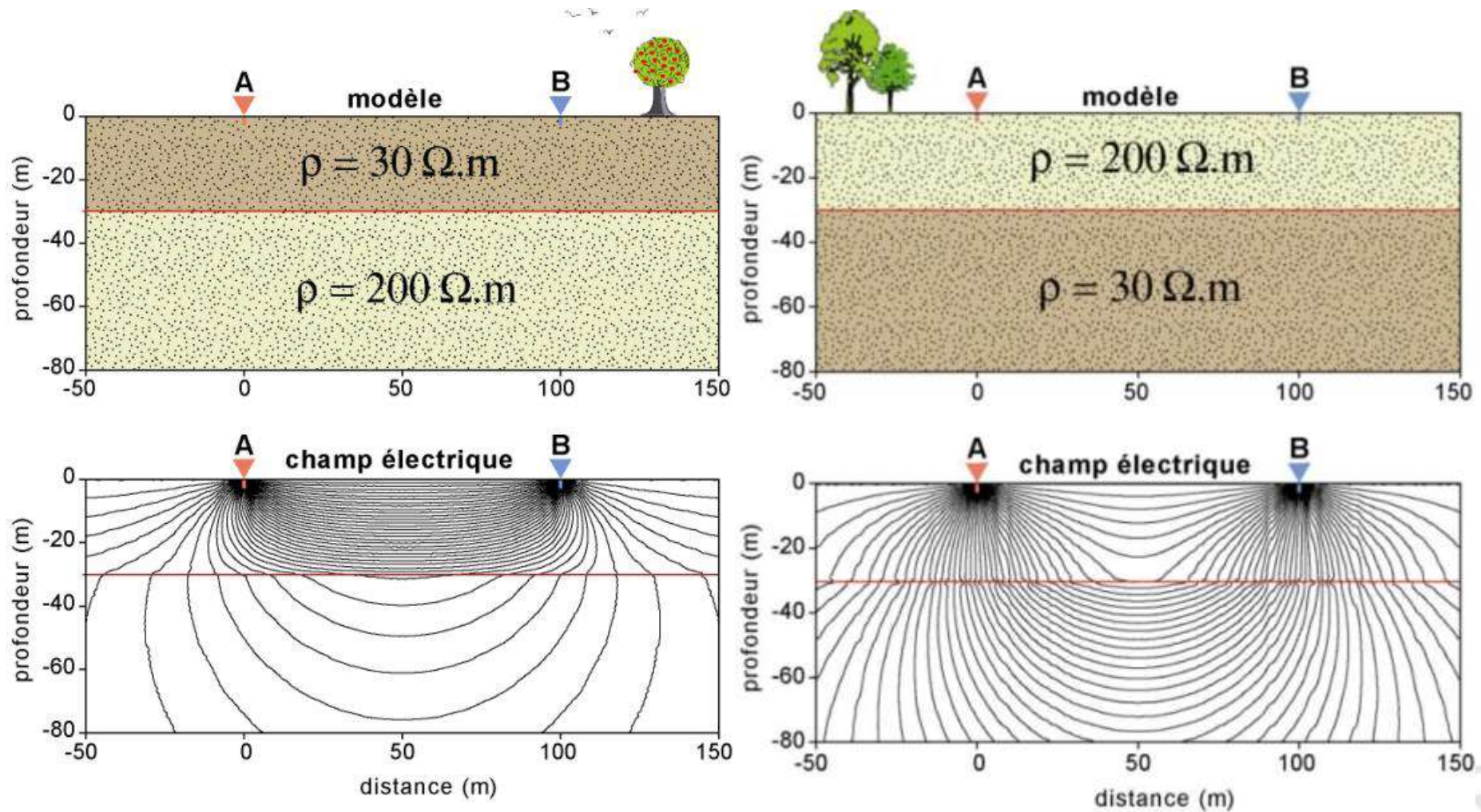


$$\rho_1 > \rho_2$$

Current Flow Lines

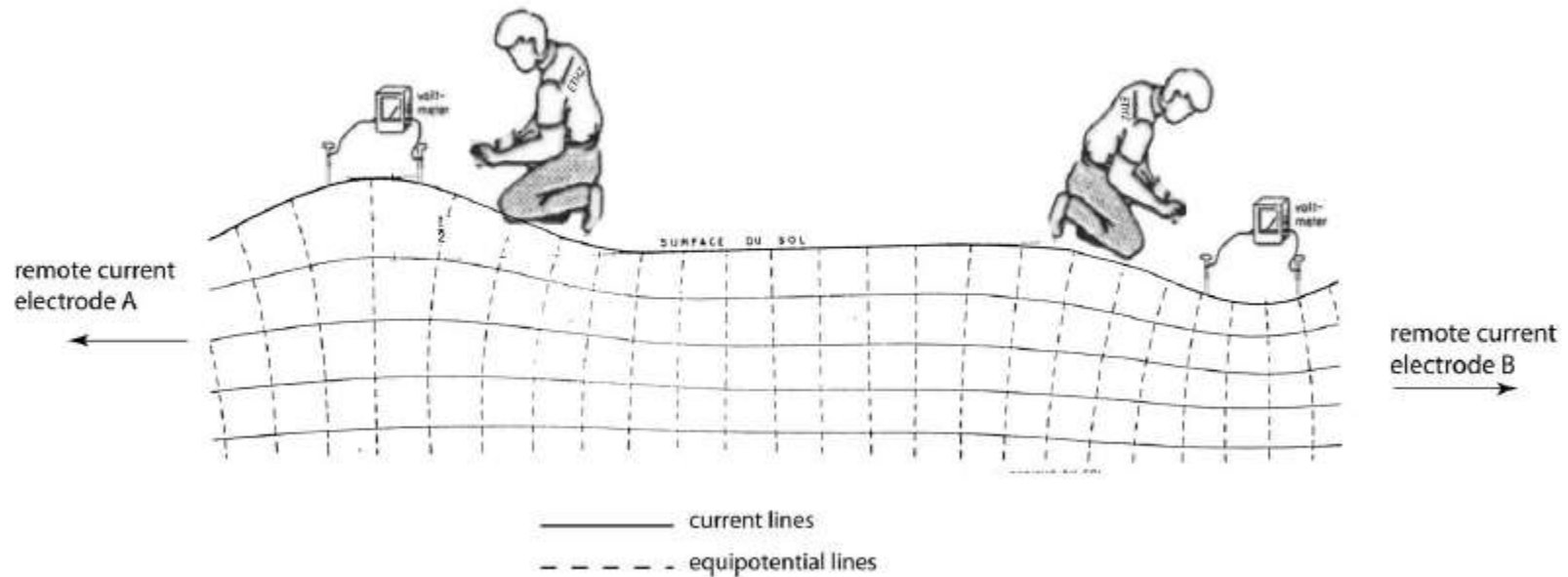


Effect of Near-Surface Resistivity



Resistivity affects depth of investigation

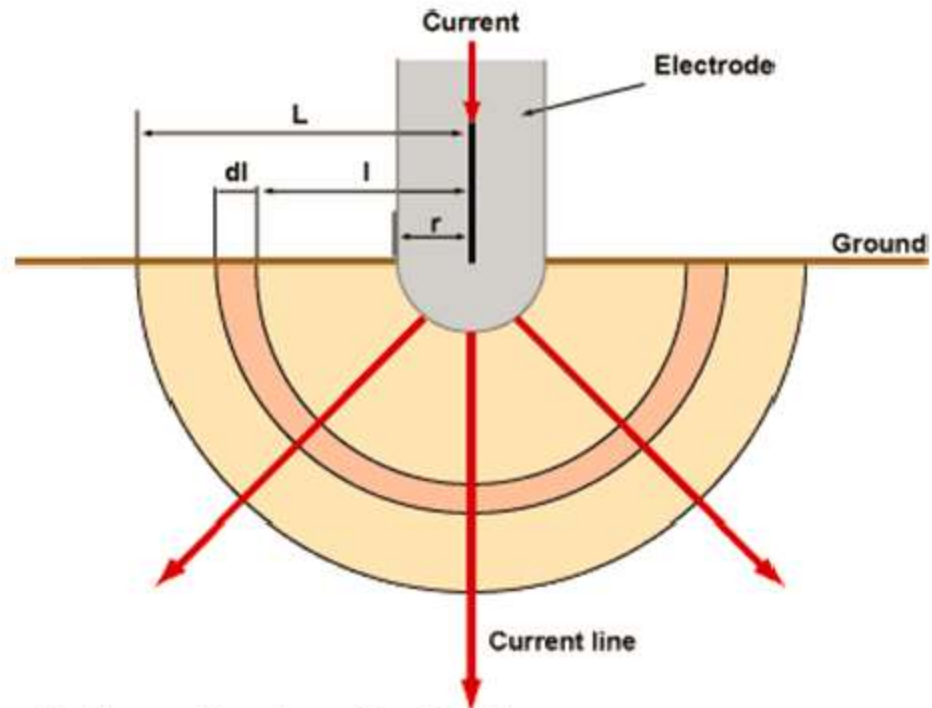
Effects of Topography



Contact Resistance

$$dR = \rho \frac{dL}{s} = \rho \frac{dL}{2\pi L^2}$$

$$R = \frac{\rho}{2\pi} \left(\frac{1}{r} - \frac{1}{L} \right)$$



L = distance to the centre of the electrode [m]

r = radius of the electrode [m]

R = resistance [ohm]

ρ = resistivity of the surrounding ground [ohm.m]

Decrease the Contact Resistance

- Add extra electrodes
- Increase current intensity
- Increase diameter of current electrodes
- Hammer electrodes deeper into the ground
- Add water to the ground around the electrodes
- Add salt to water

Approx. 90% of the contact resistance contribution comes from a portion of the ground around the electrode that is equal to 10 times the diameter of the electrode.

Coping with Noise

- Telluric Currents
- Man-made currents
- Metallic conductors in the ground

Solutions:

- Use Alternating Currents
- Stack the data
- Rejection filters

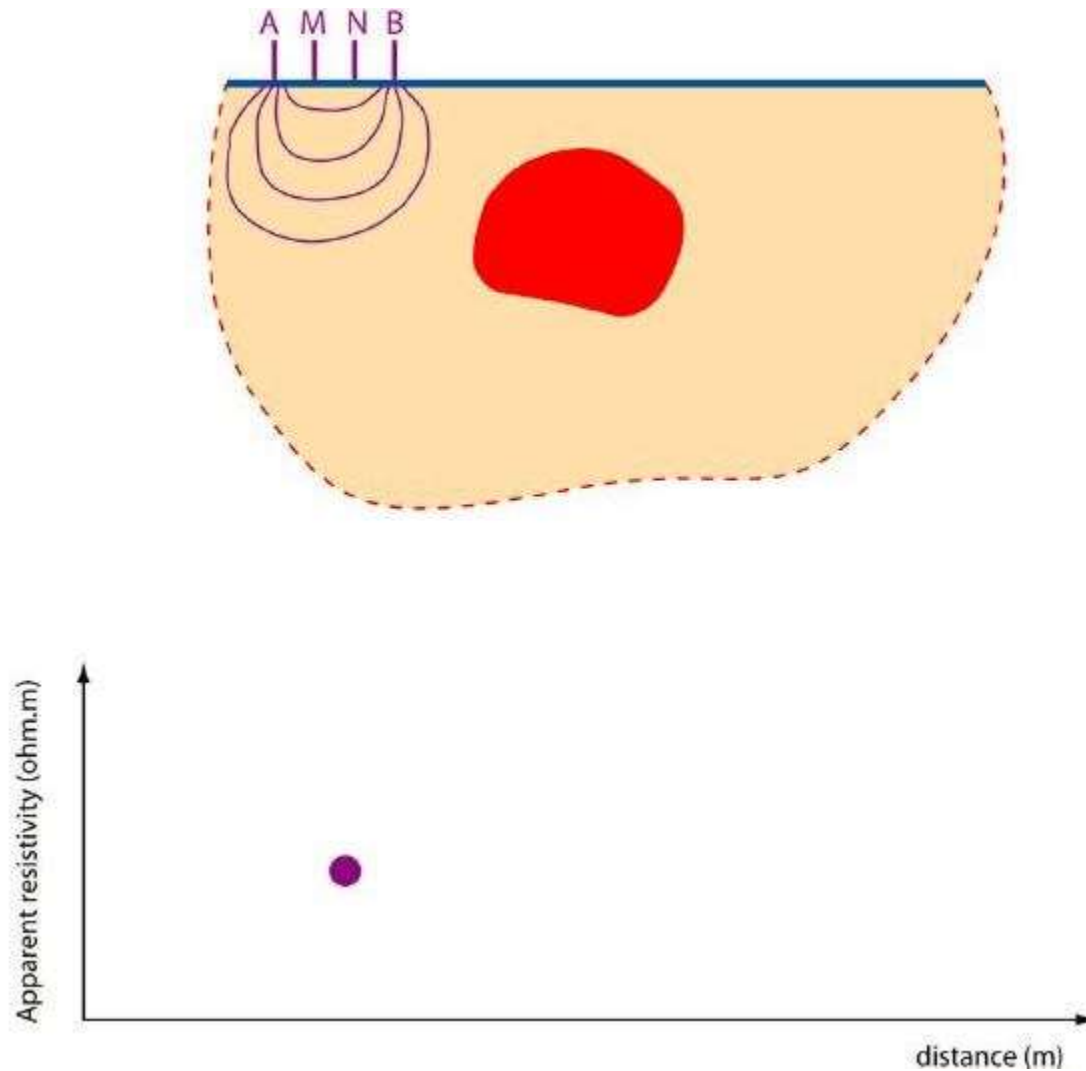
PART 3 – DC Resistivity Surveys

1. Types of Surveys
2. Constant Separation Traversing (CST)
3. Vertical Electrical Sounding (VES)
4. Field Sheets

Types of Surveys

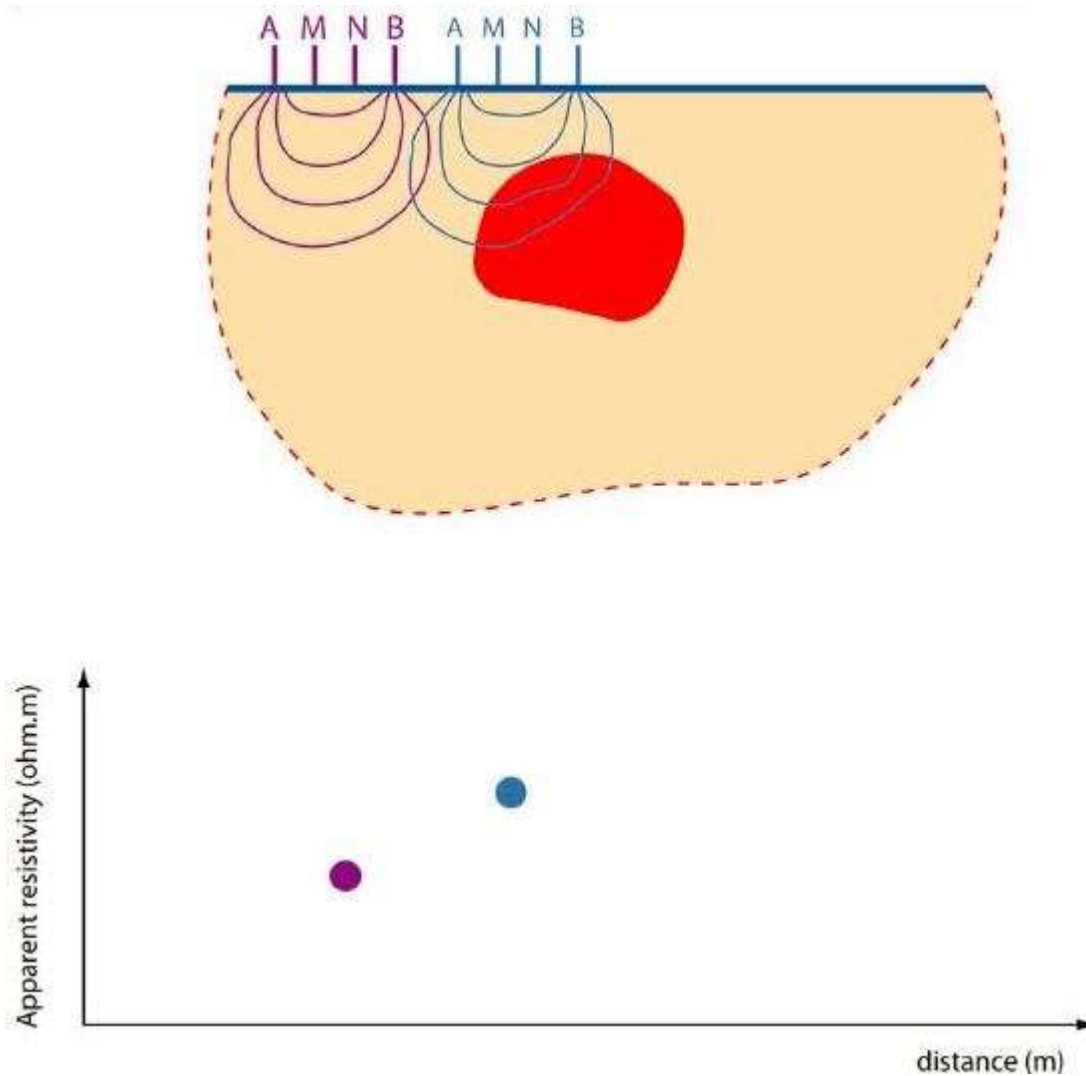
1. **Constant Separation Traversing (CST):** resistivity mapping along profiles to find lateral anomalies in resistivity. Current & Potential electrode separation is fixed, and move along the profile.
2. **Vertical Electrical Sounding (VES):** vertical resistivity mapping. The electrode spread is expanded about a central point.
3. **Electrical Resistivity tomography (ERT),** also known as Electrical Imaging, is a combination of CST & VES.

Constant Separation Traversing (CST)



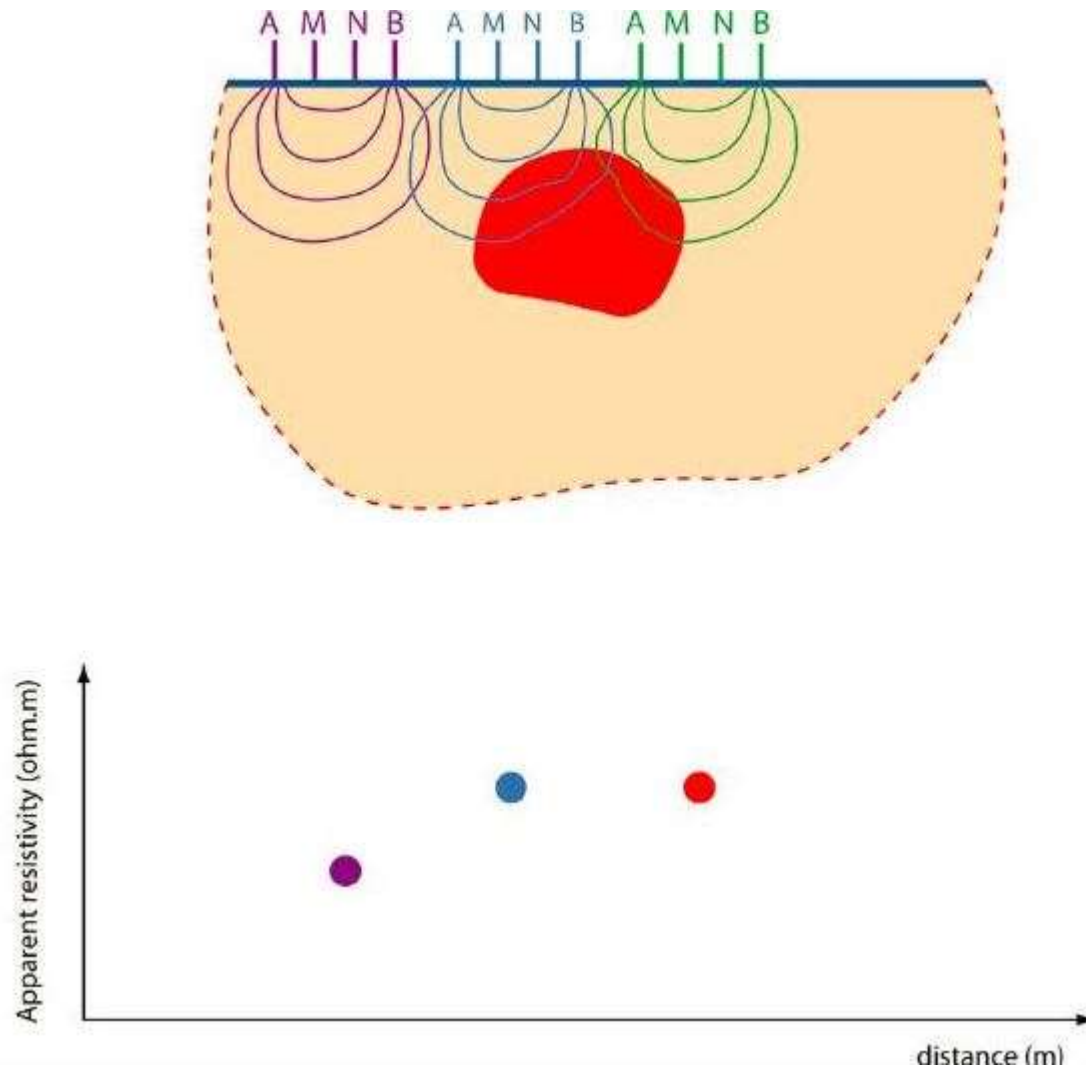
Source: http://www.tomoquest.com/Lectures_in_Geophysics.php

Constant Separation Traversing (CST)



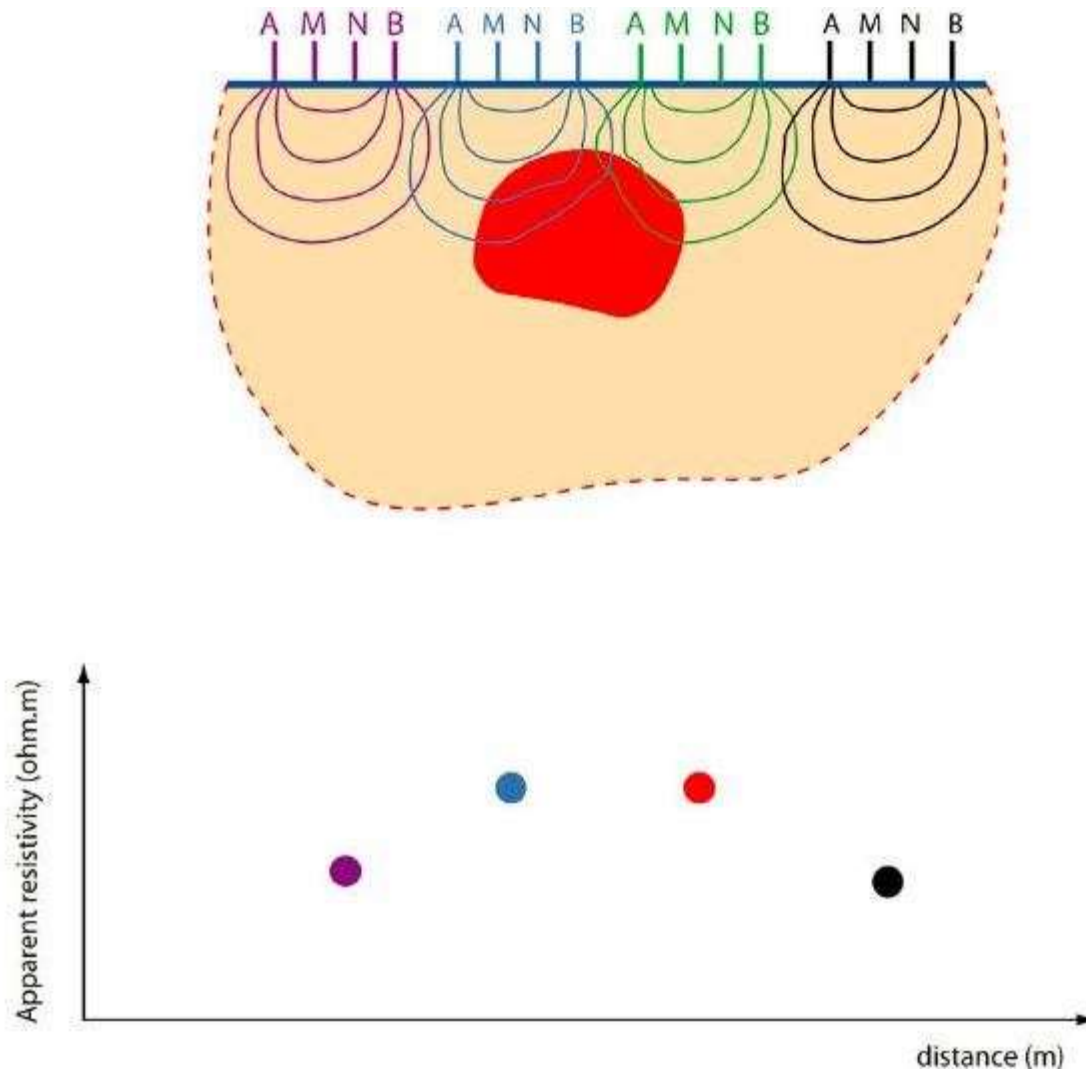
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Constant Separation Traversing (CST)



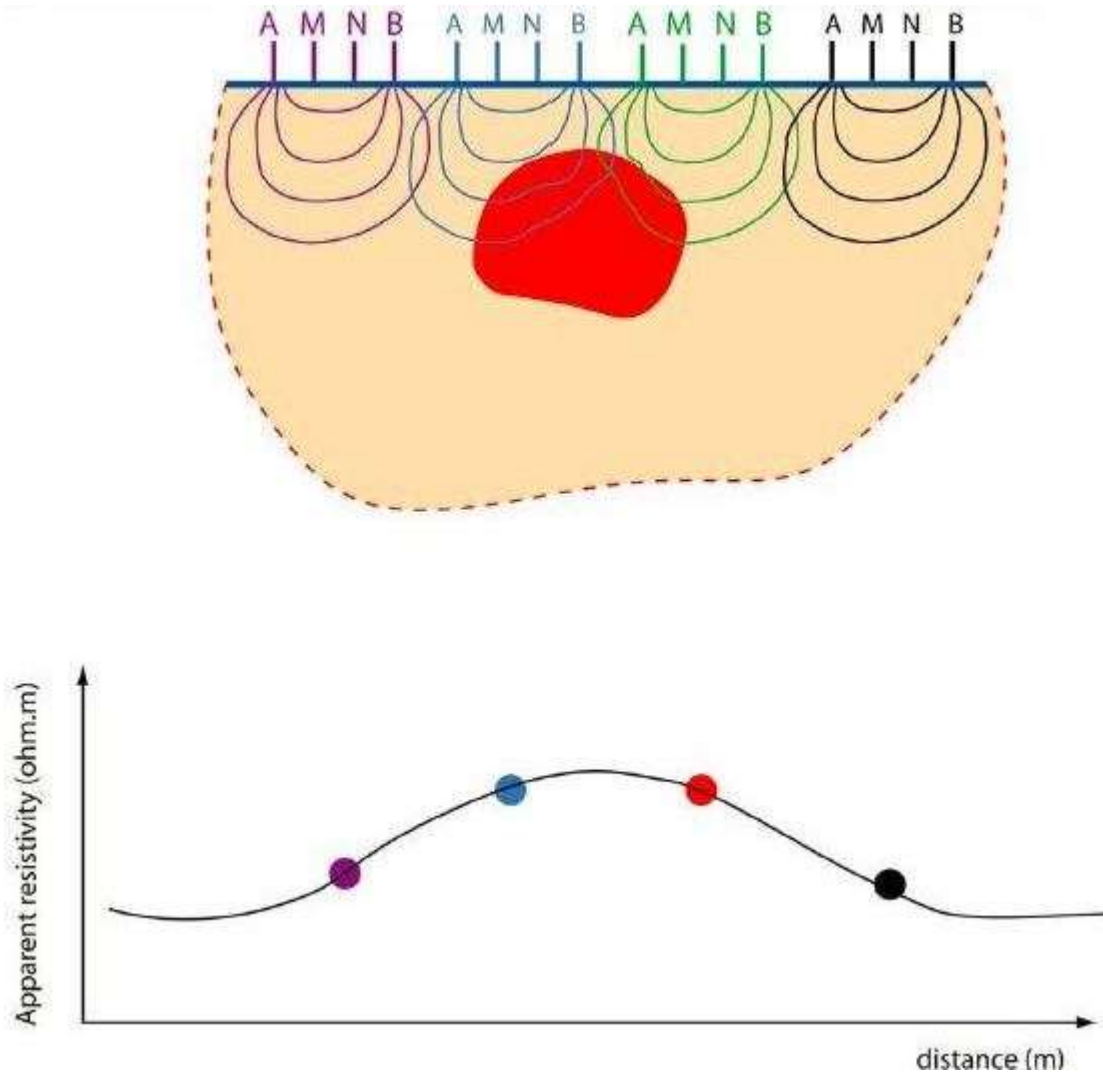
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Constant Separation Traversing (CST)



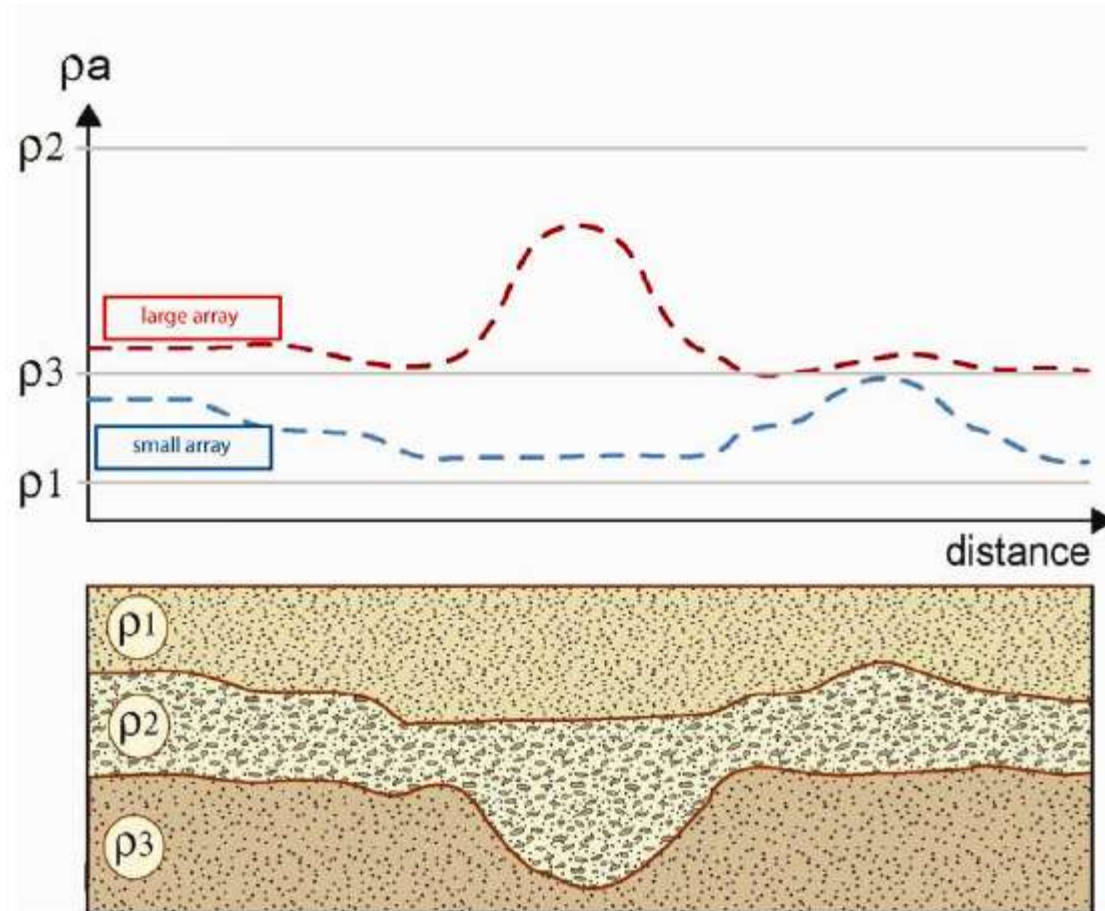
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Constant Separation Traversing (CST)

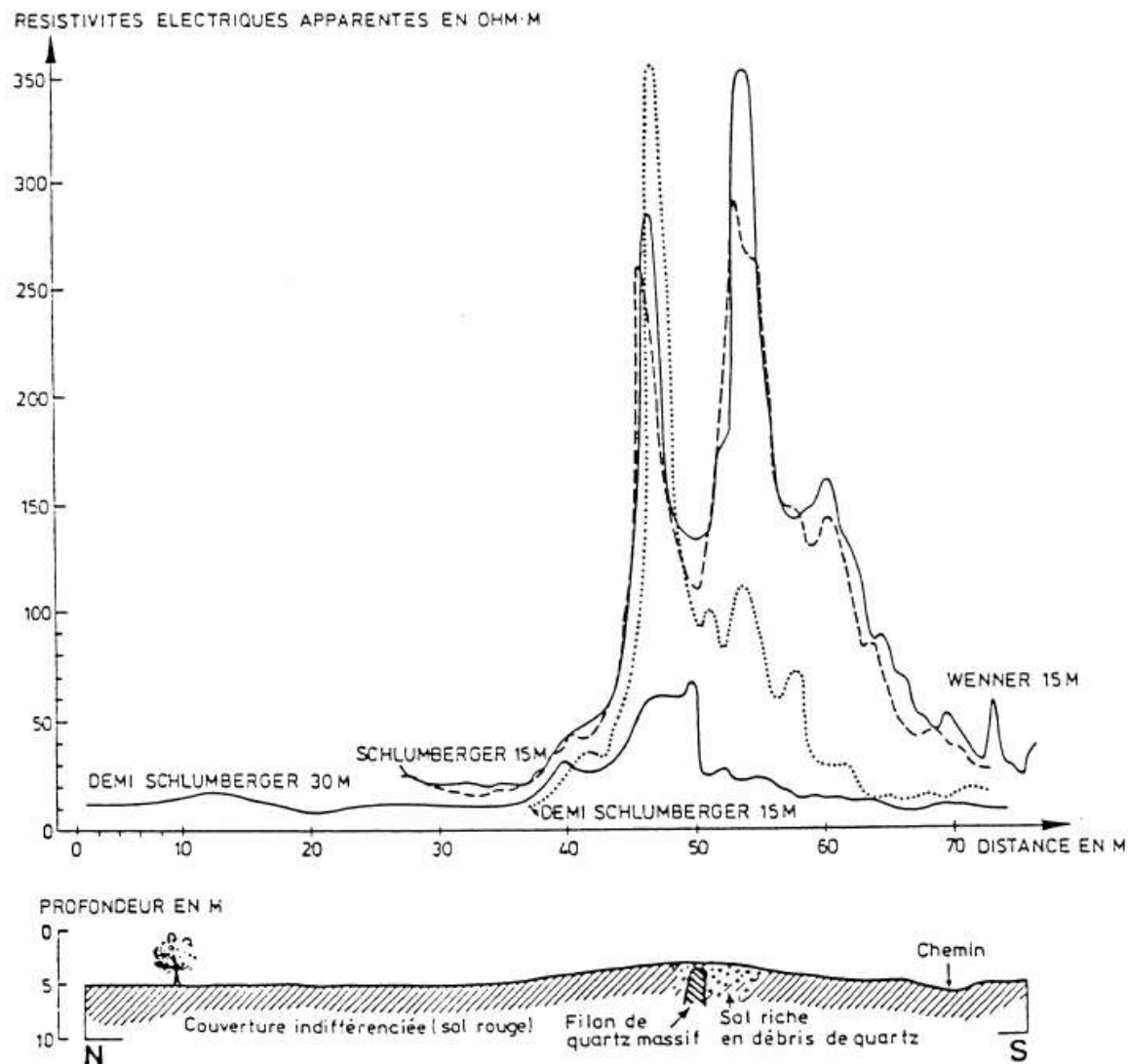


Source: http://www.tomoquest.com/Lectures_in_Geophysics.php

Interpretation of CST



Interpretation of CST



Source: http://www.tomoquest.com/Lectures_in_Geophysics.php

Resistivity Traversing

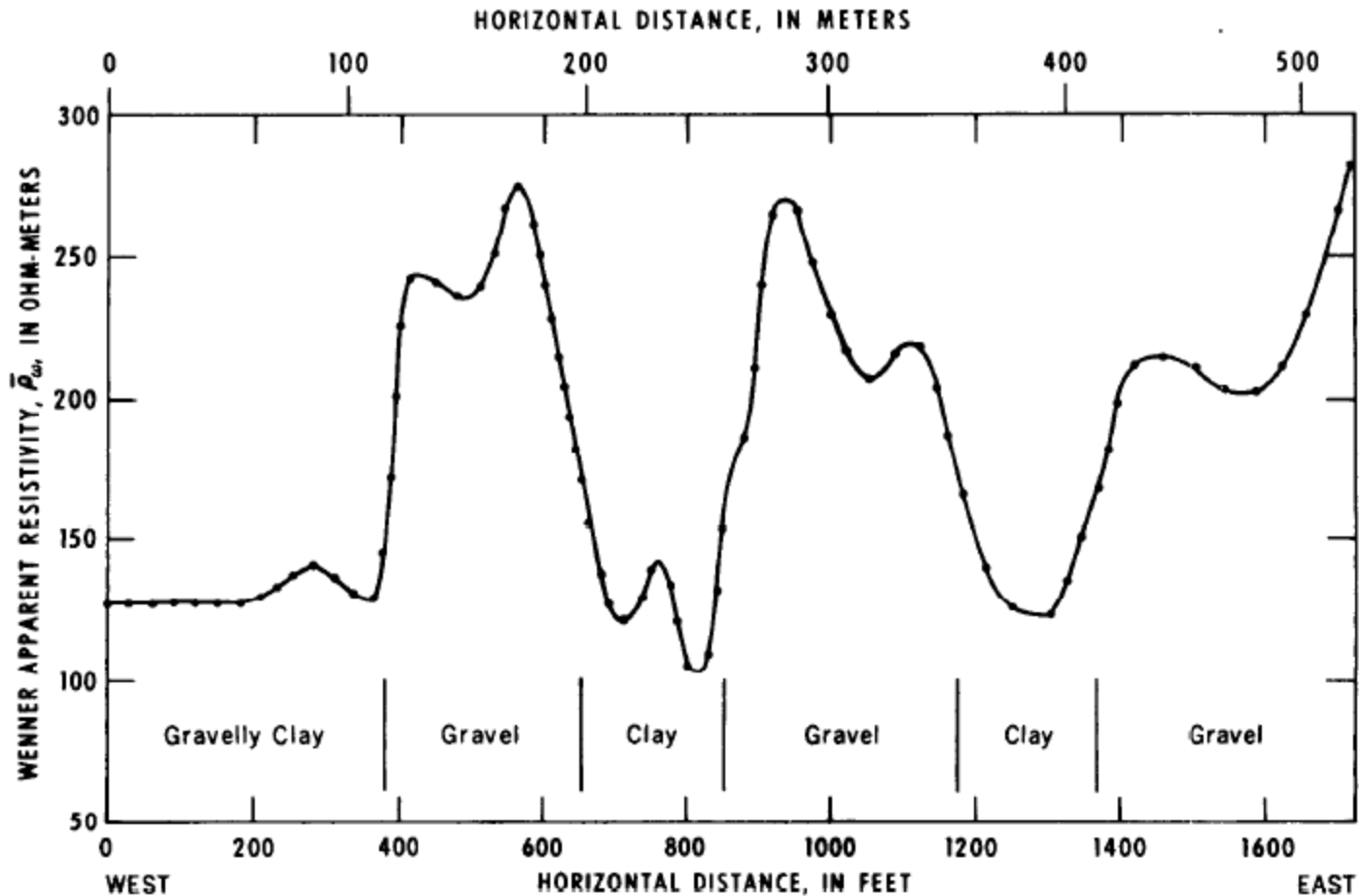


Figure 7.—Horizontal profile and interpretations over a shallow gravel deposit in California (Zohdy, unpub. data, 1964; Zohdy, 1964) using Wenner array at $a = 9.15$ meters.

Apparent Resistivity Map

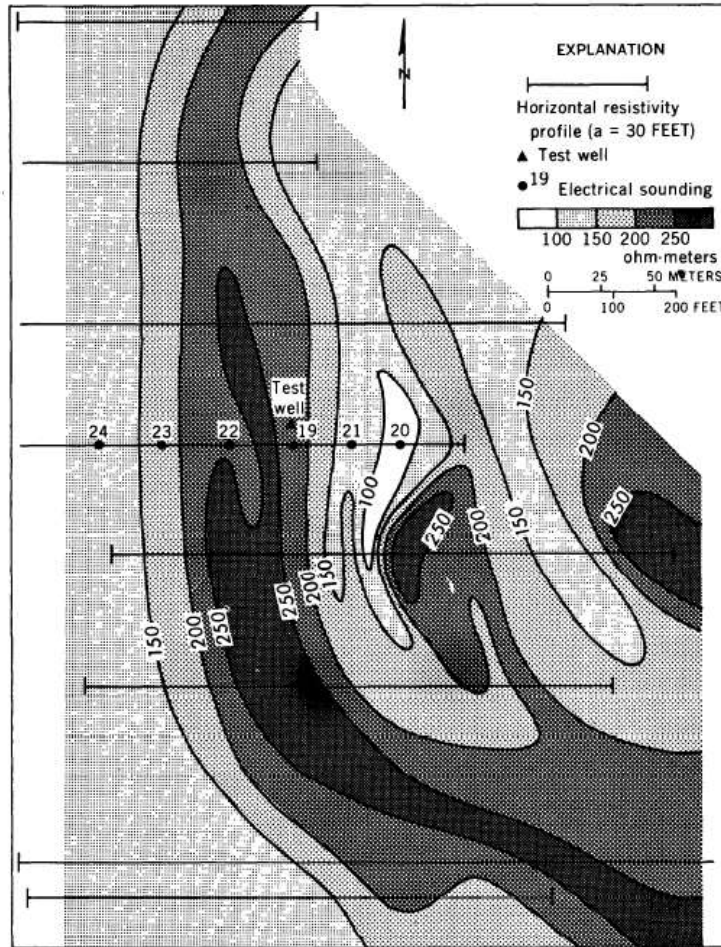


Figure 8.—Apparent-resistivity map near Campbell, Calif. Unpublished data obtained by Zehdy (1964) using Wenner array. Crosshatched areas are buried stream channels containing thick gravel deposits. Stippled areas are gravelly clay deposits.

Resistivity Profile over Buried Stream Channel

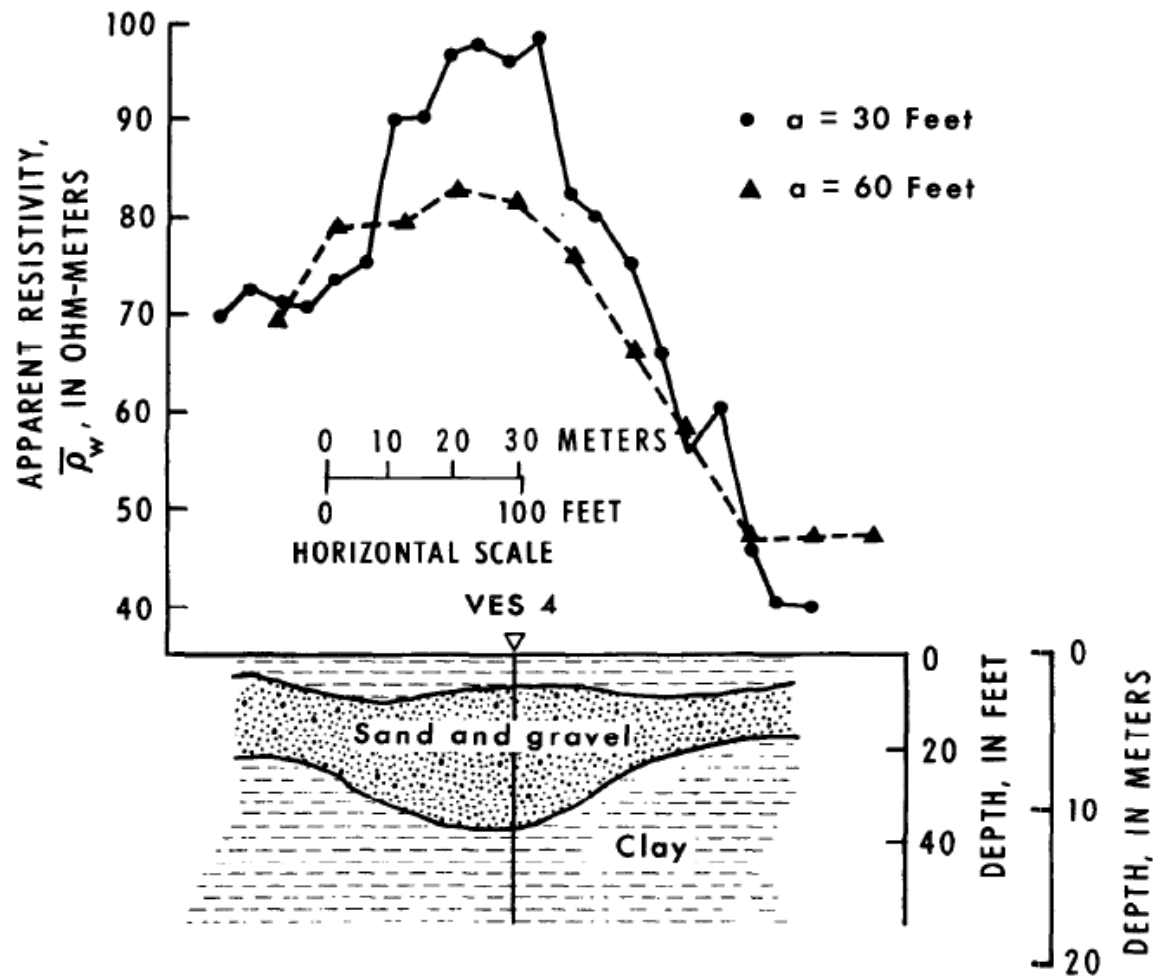


Figure 9.—Horizontal profiles over a buried stream channel using two electrode spacings: $a = 9.15$ meters (30 feet) and $a = 18.3$ meters (60 feet) (after Zohdy, 1964). VES 4 marks the location of an electrical sounding used to aid in the interpretation of the profiles.

Mapping Buried Stream Channels

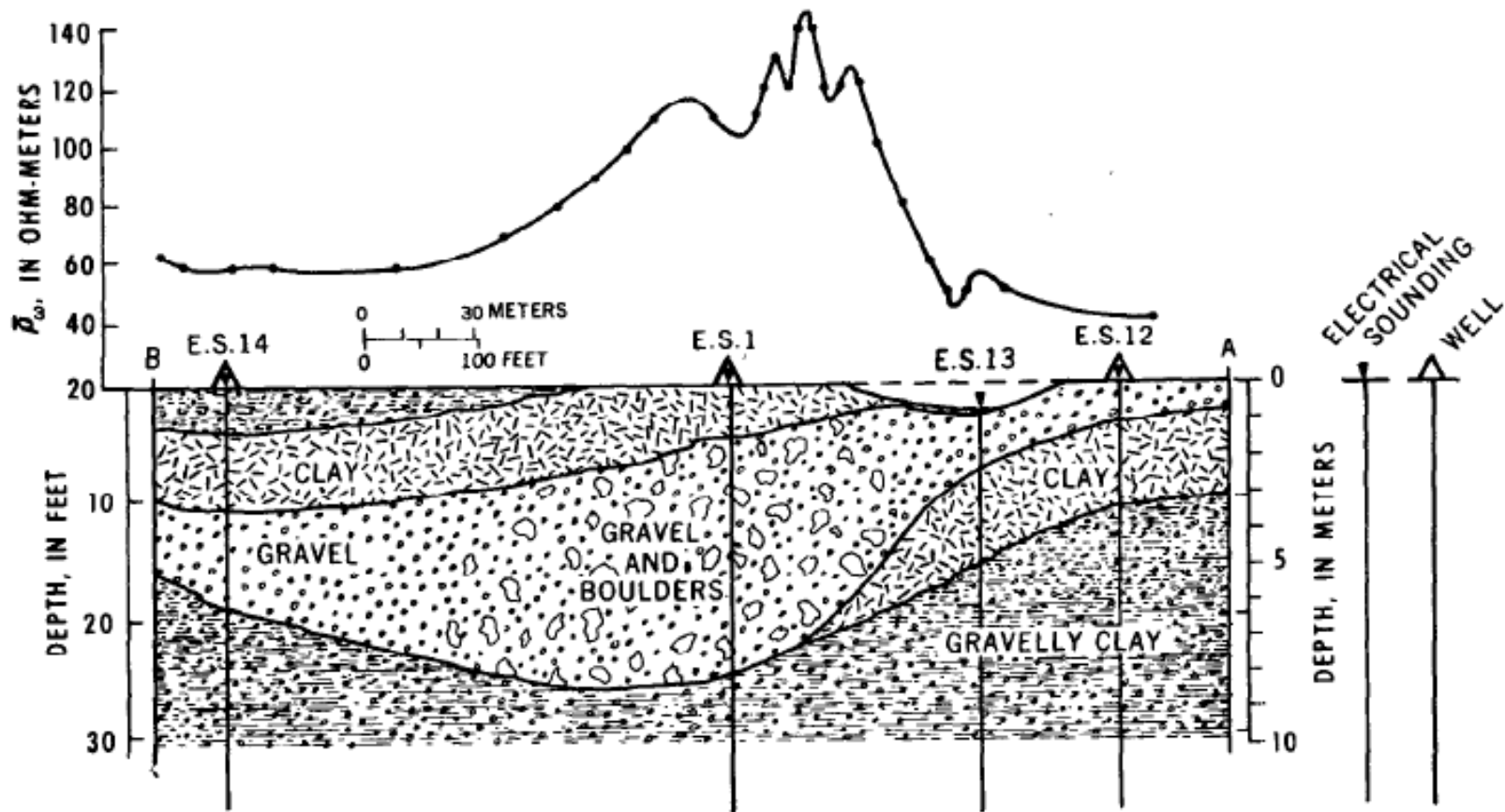


Figure 39.—Resistivity profile and geologic section, Penitencia, Calif. (after Zohdy, 1964, 1965). Horizontal profile obtained using Wenner array with electrode spacing $a = 6.1$ m (20 feet).

Mapping Buried Stream Channels

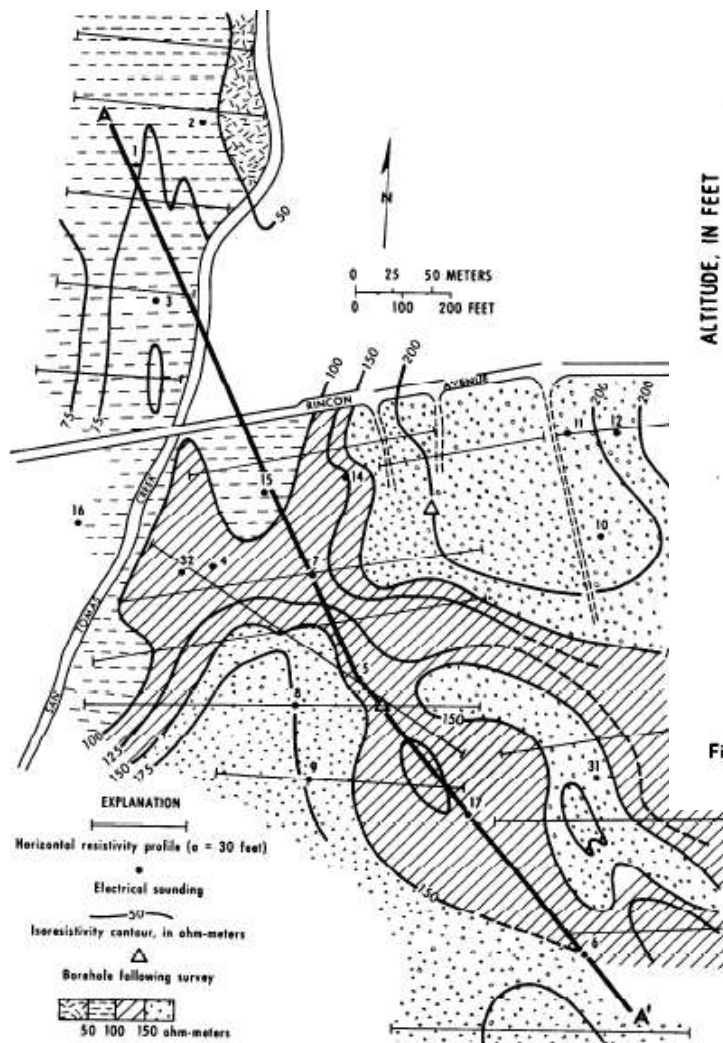


Figure 40.—Map of apparent resistivity near Campbell, Calif., obtained with Wenner array at $a = 9.15$ m (30 feet) and showing location of section AA'. (Unpub. data obtained by Zohdy, 1964.)

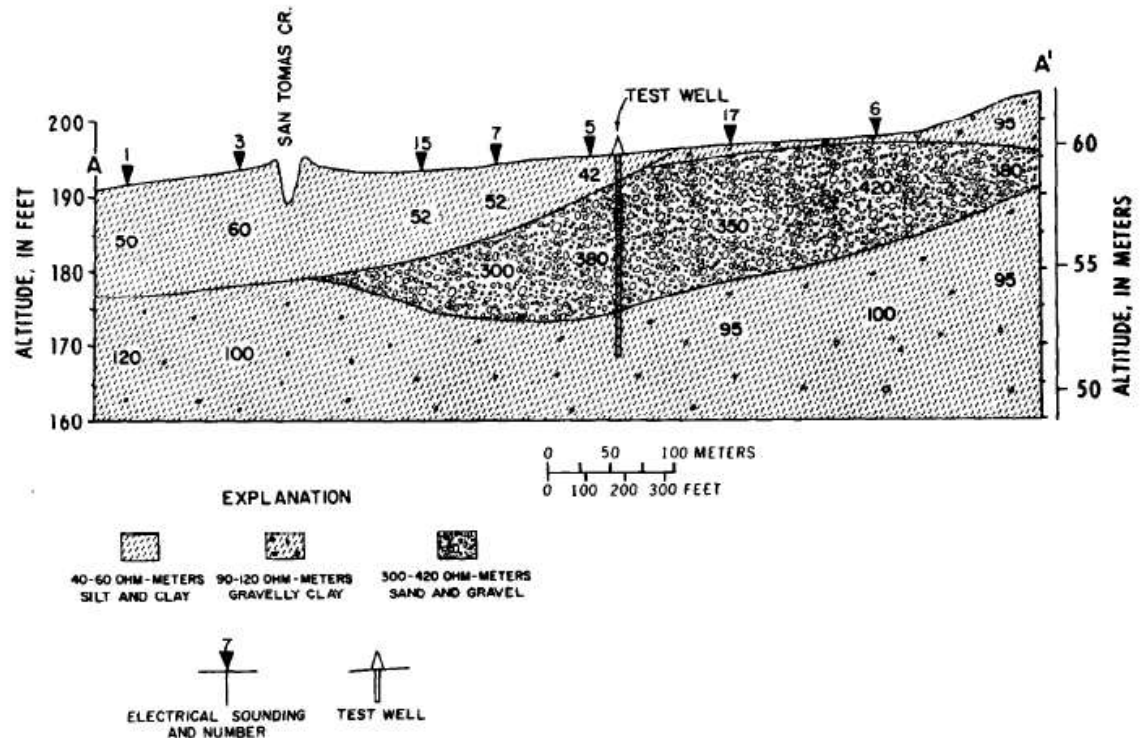


Figure 41.—Geoelectric section and drilling results near Campbell, Calif. Numbers in layers designate interpreted true resistivities. (Unpub. data obtained by Zohdy, 1964.)

Mapping Buried Stream Channels

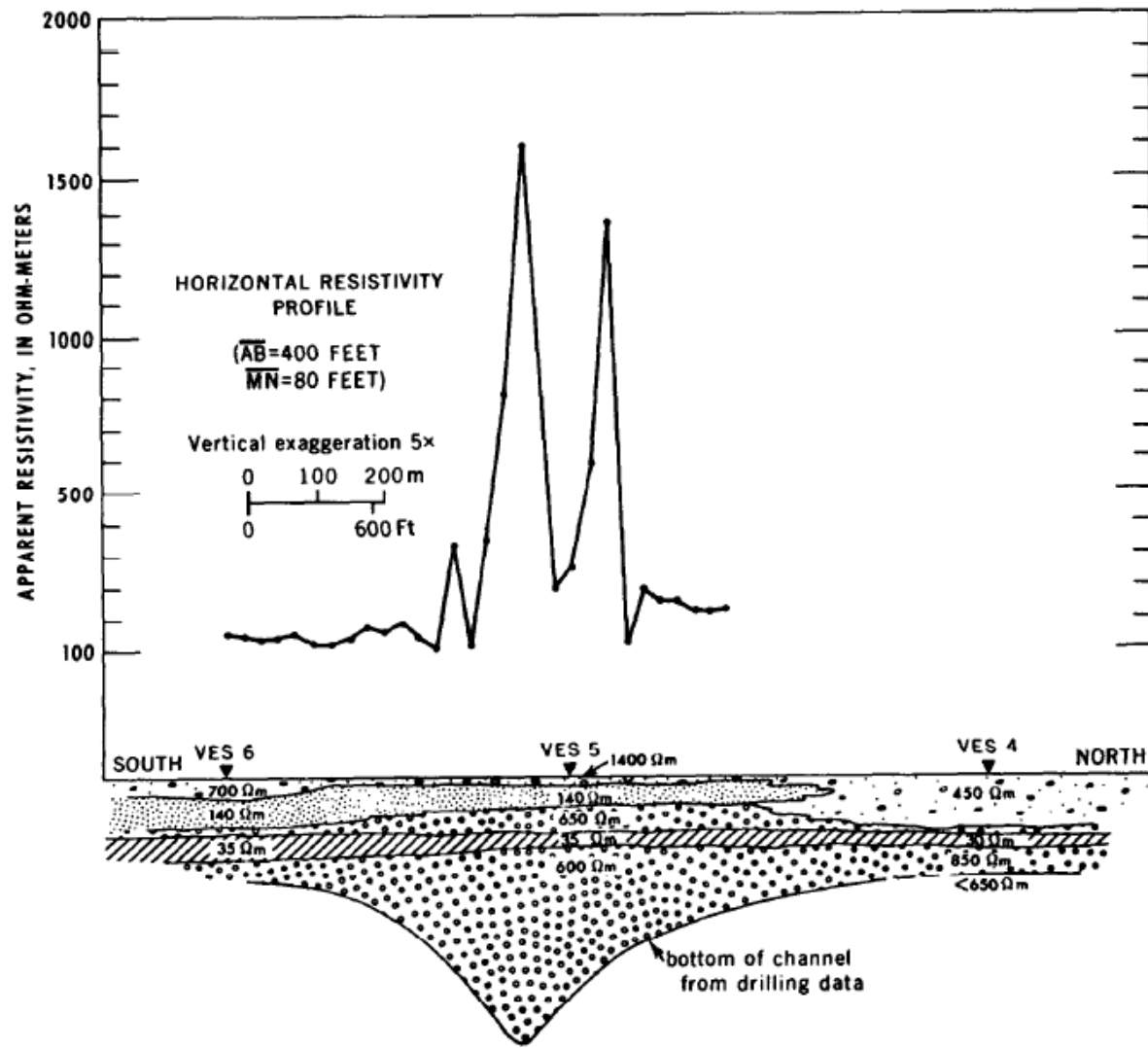
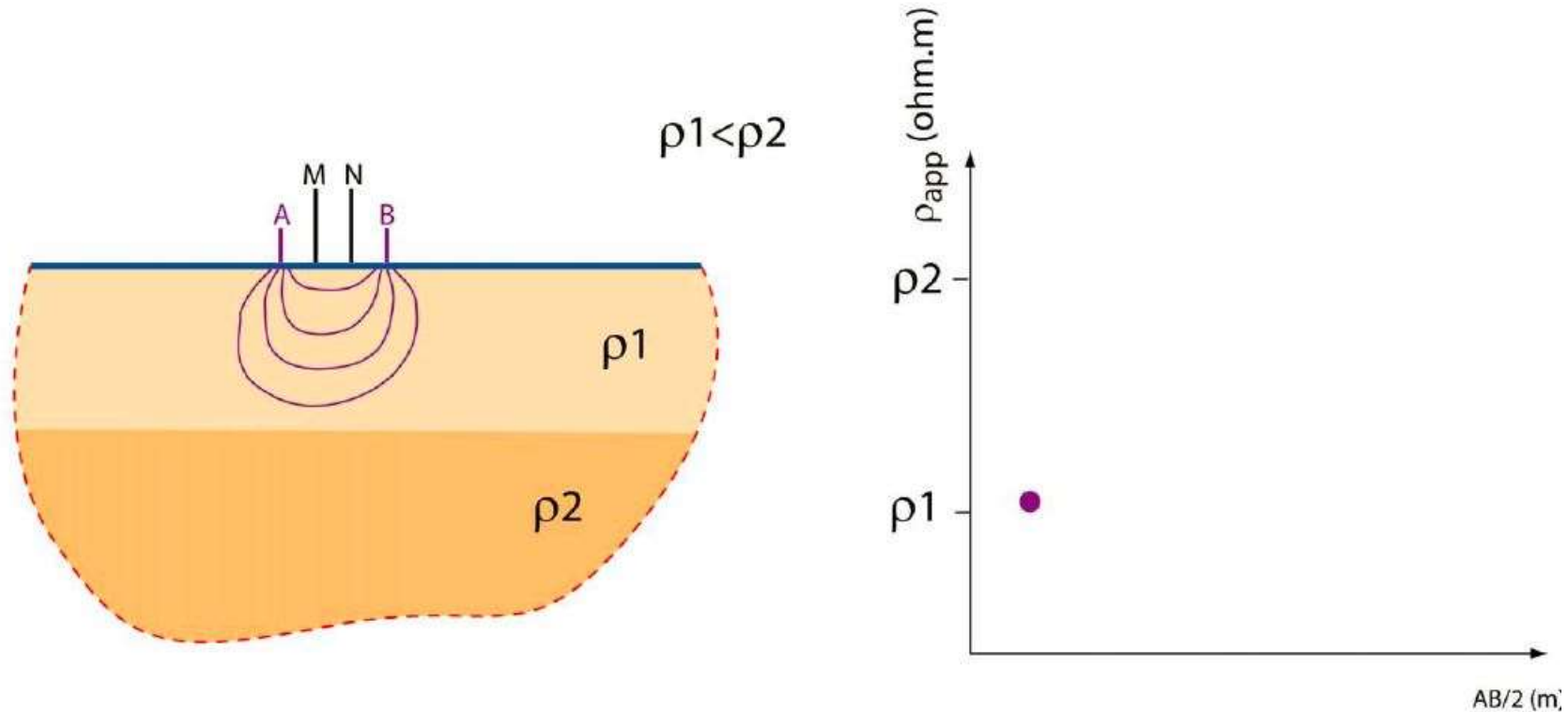
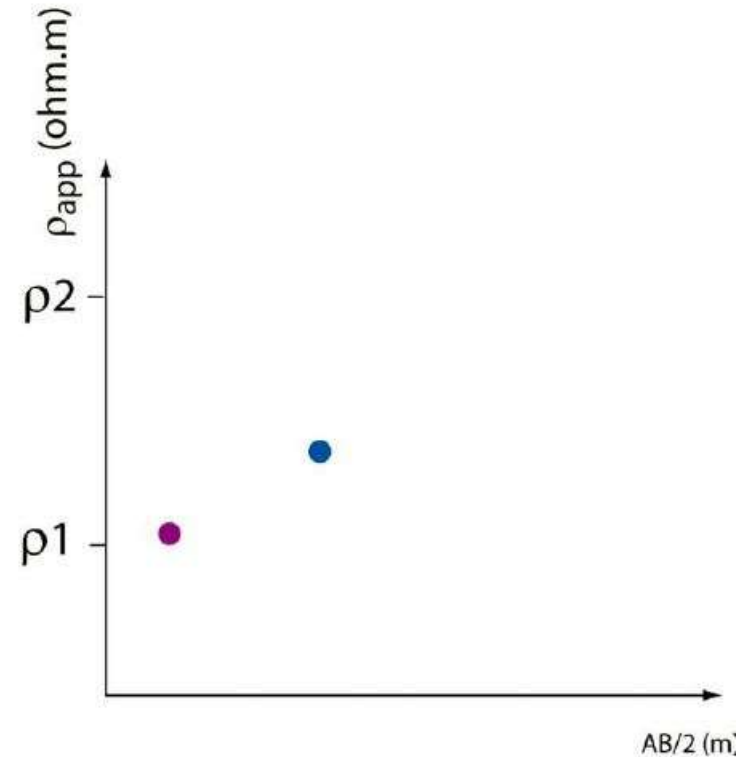
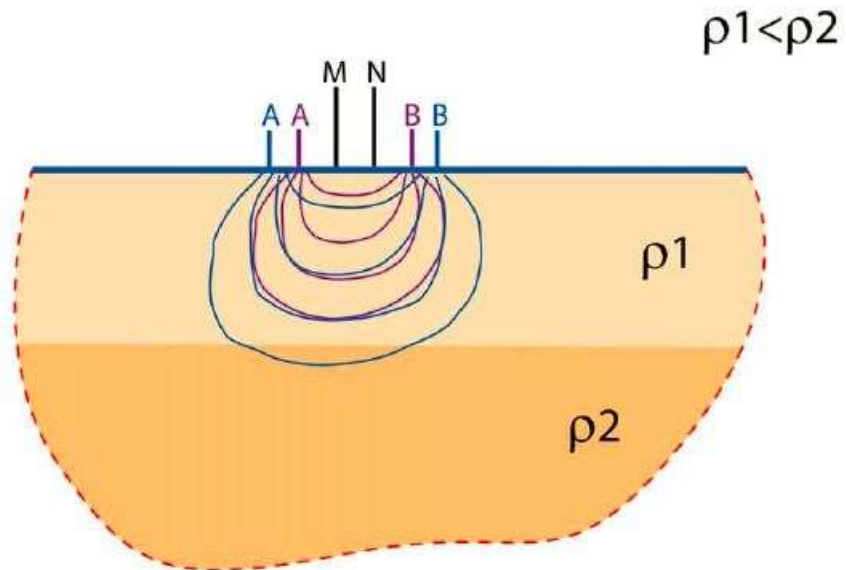


Figure 42.—Apparent-resistivity profile and geologic interpretation over buried channel, near Salisbury, Md. Data obtained by Zohdy and Jackson in 1966.

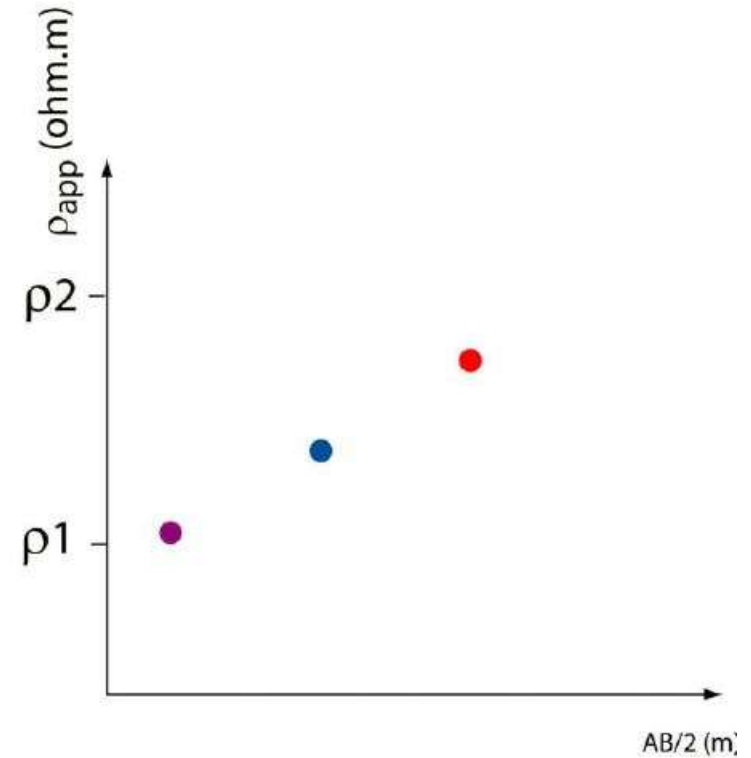
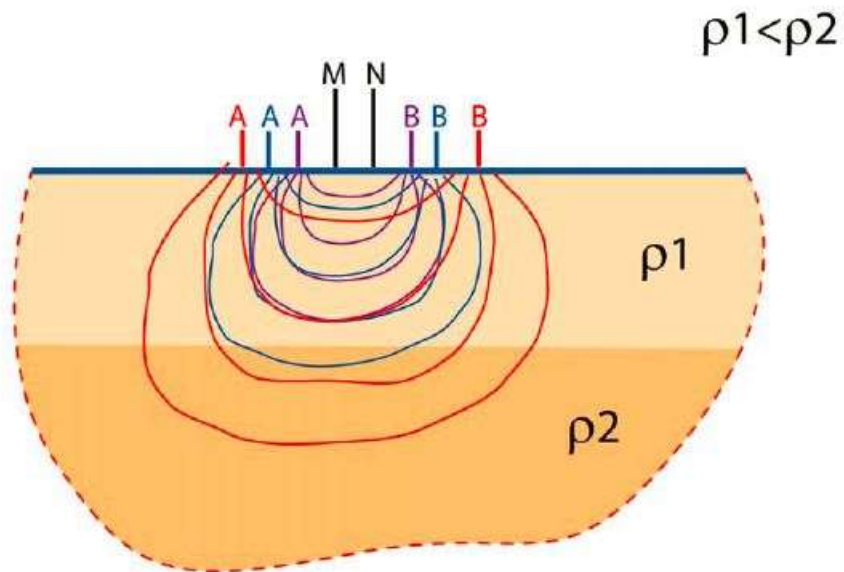
Vertical Electrical Sounding (VES)



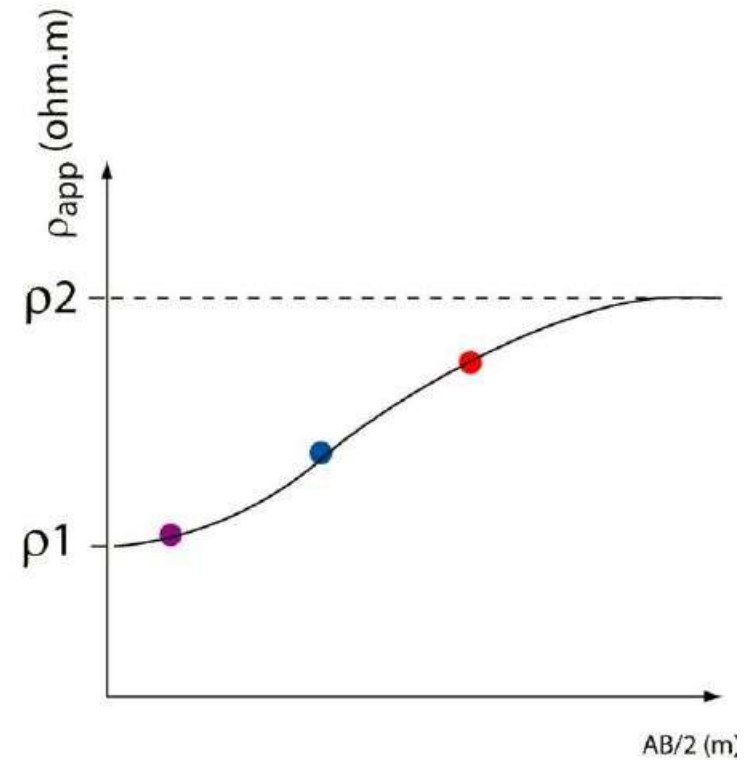
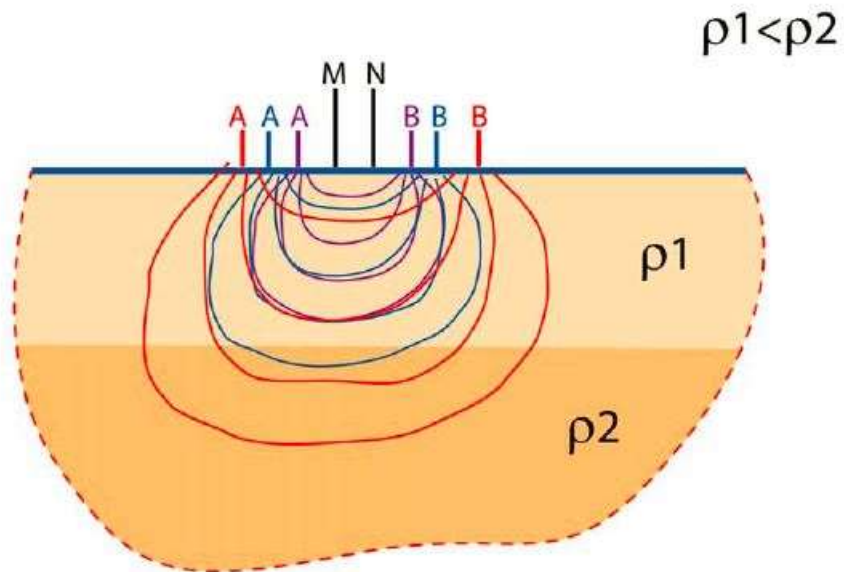
Vertical Electrical Sounding (VES)



Vertical Electrical Sounding (VES)



Vertical Electrical Sounding (VES)



DC Resistivity Field Sheets - Schlumberger



SCHLUMBERGER ARRAY FIELD SHEET

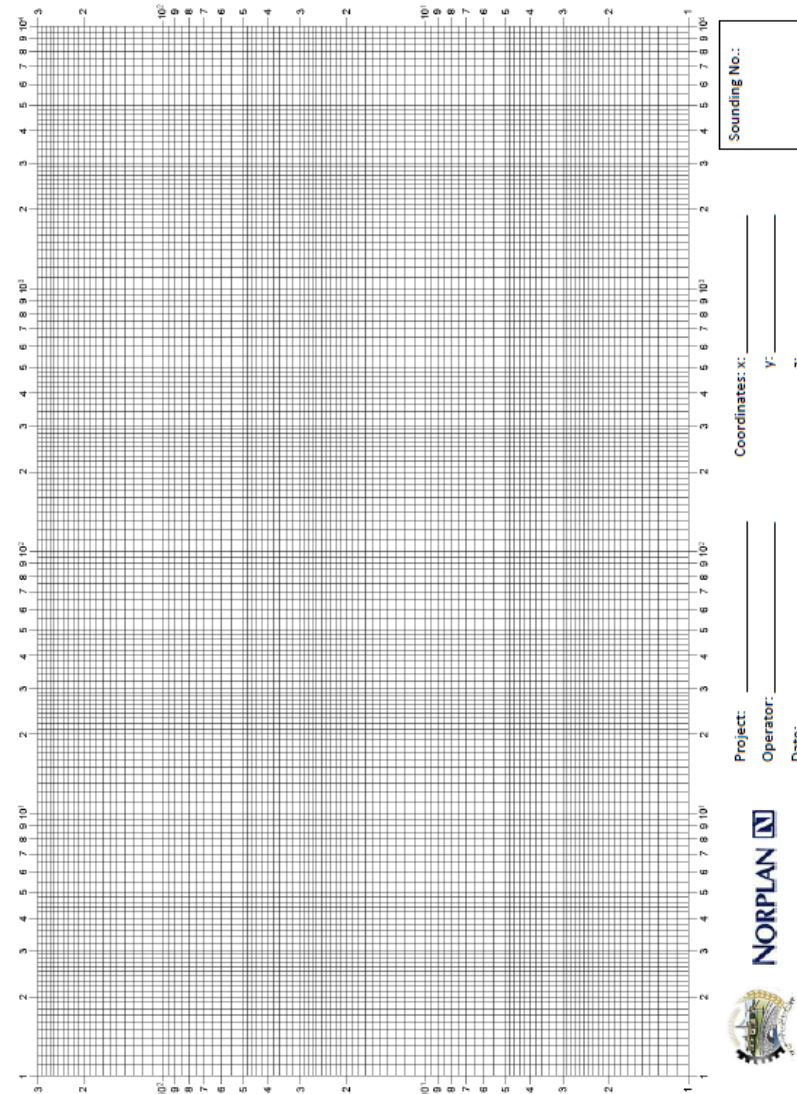
NORPLAN

Project: _____ Sounding No.: _____
 Location: _____ Coordinates East: _____
 Equipment: _____ Coordinates North: _____
 Operator: _____ Azimuth: _____

$$\rho_a = K \frac{\Delta V}{I}$$

$$\rho_a = K \frac{\Delta V}{I}$$

Marks	OA in m	K for				ΔV in millivolts (mV)	I in milliamperes (mA)	ρ_a in ohm-m (Ω m)
		M N 1m	M N 10m	M N 60m	M N 200m			
1	1	2.35						
2	2	11.8						
3	3	27.5						
1	4	49.5						
2	5	77.7						
3	6	112						
1	8	200						
2	10	313						
3	15	705	62.8					
1	20	1250	118					
2	25	1960	188					
3	30	2820	275					
1	35	3850	377					
2	40	5020	495					
3	50	7850	780					
1	60	11300	1120					
2	70	15400	1530					
3	80	20100	2000	288				
1	100	31400	3130	475				
2	125		4900	770				
3	150		7050	1130				
1	175		9600	1560				
2	200		12500	2040				
3	250		19600	3230				
1	300		28200	4660				
2	350			6360	1766			
3	400			8300	2360			
1	450			10500	3000			
2	500			13000	3760			



NORPLAN

PART 4 – VES Interpretation

1. Schlumberger – Wenner comparison
2. One & Two Layer Models
3. Three Layer Models
4. Effects of Inhomogeneity
5. Correcting Sounding Curves
6. Principle of Equivalence
7. Principle of Suppression

Comparison: Wenner & Schlumberger Arrays

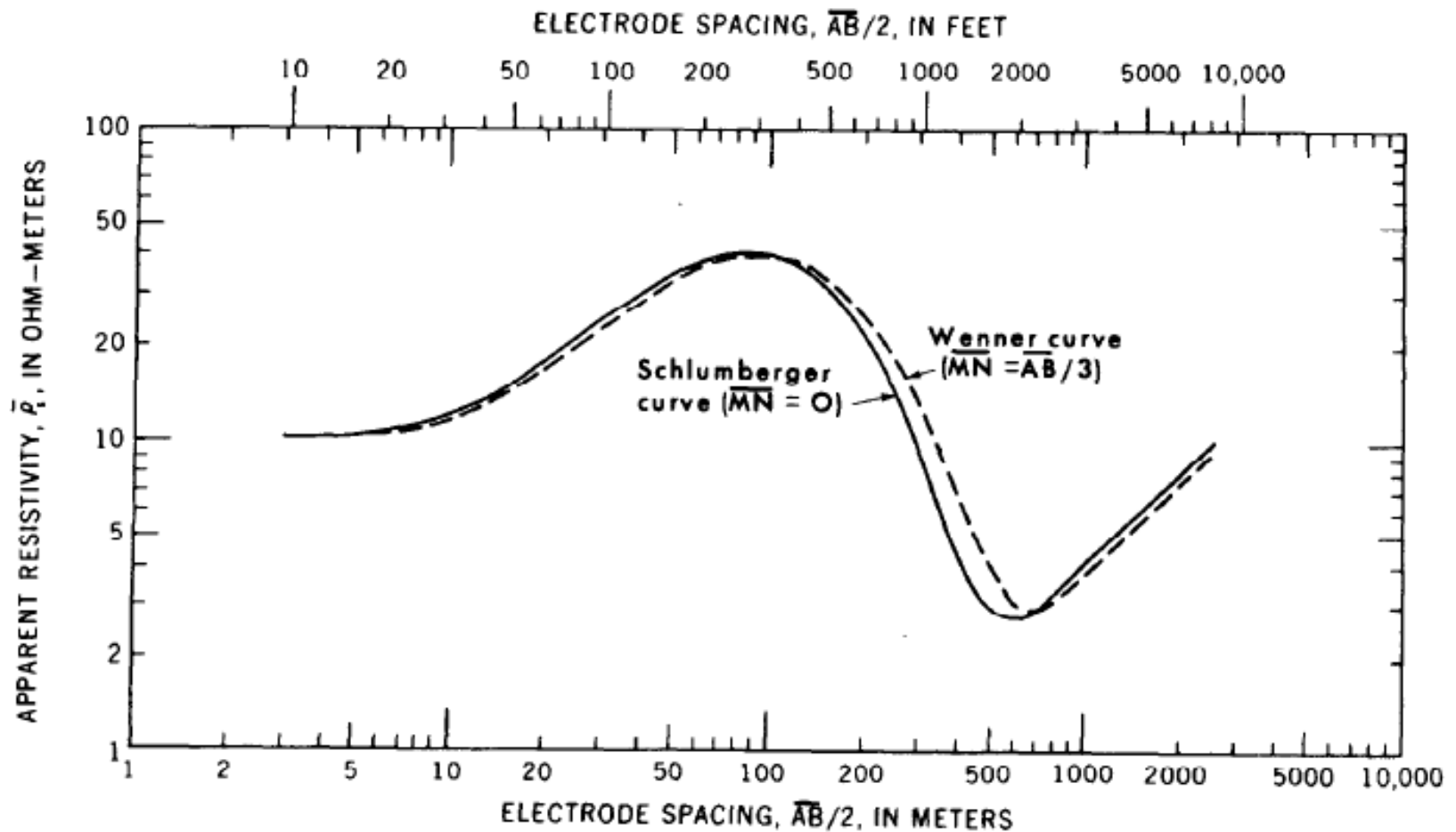
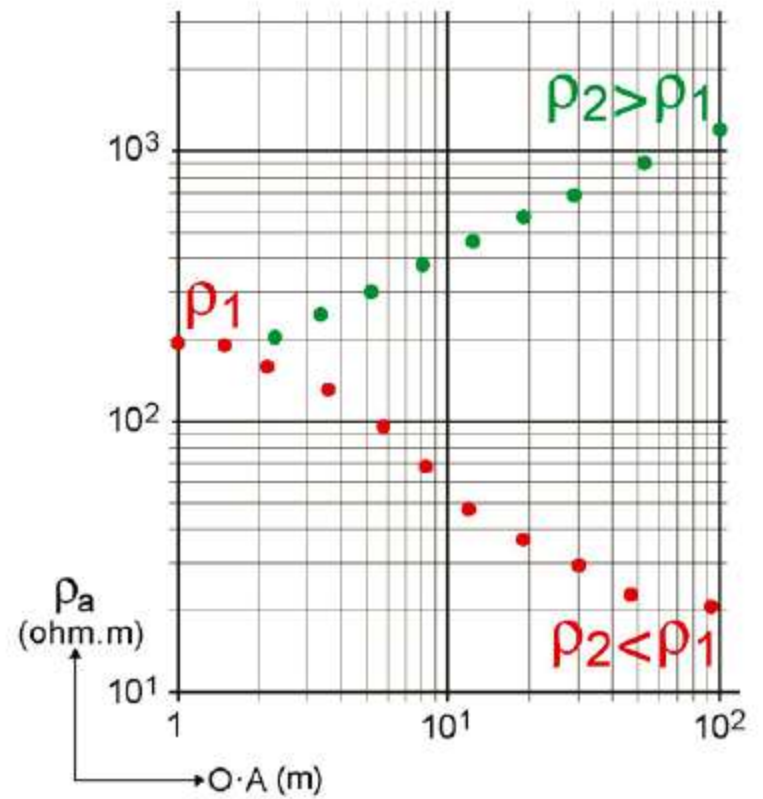
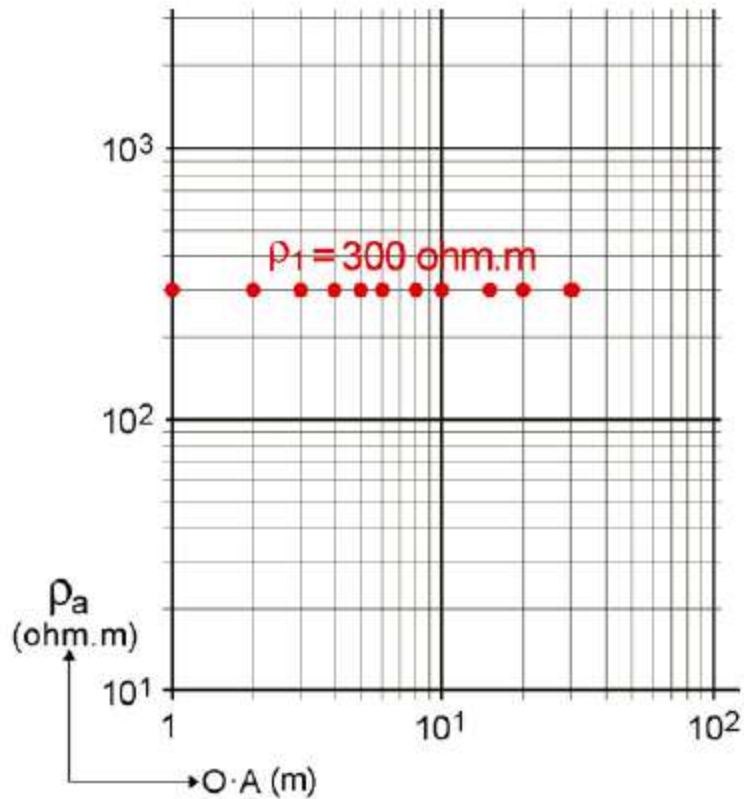
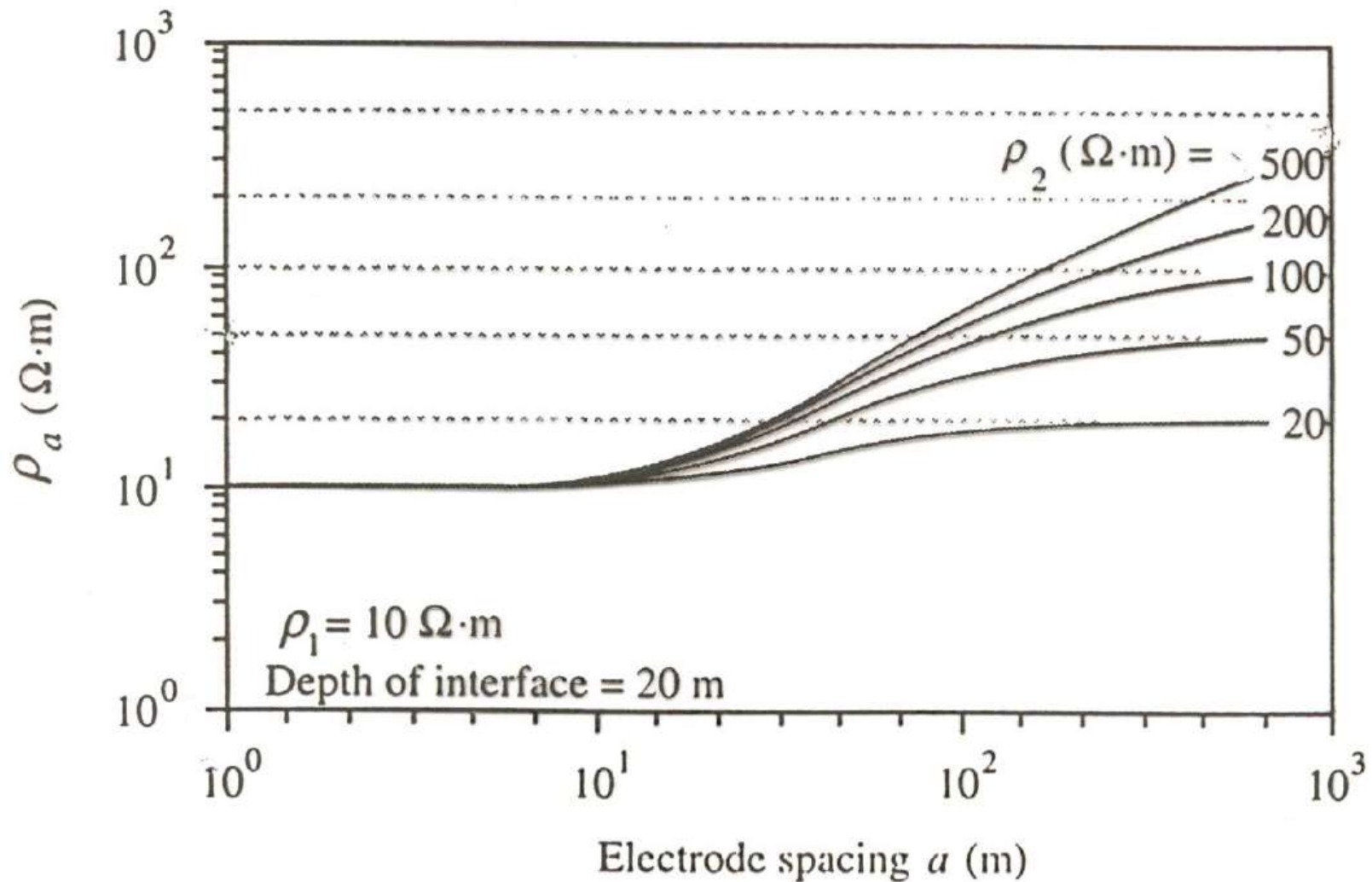


Figure 11.—Comparison between four-layer Schlumberger and Wenner sounding curves. Electrode spacing is $\overline{AB}/2$ for both curves.

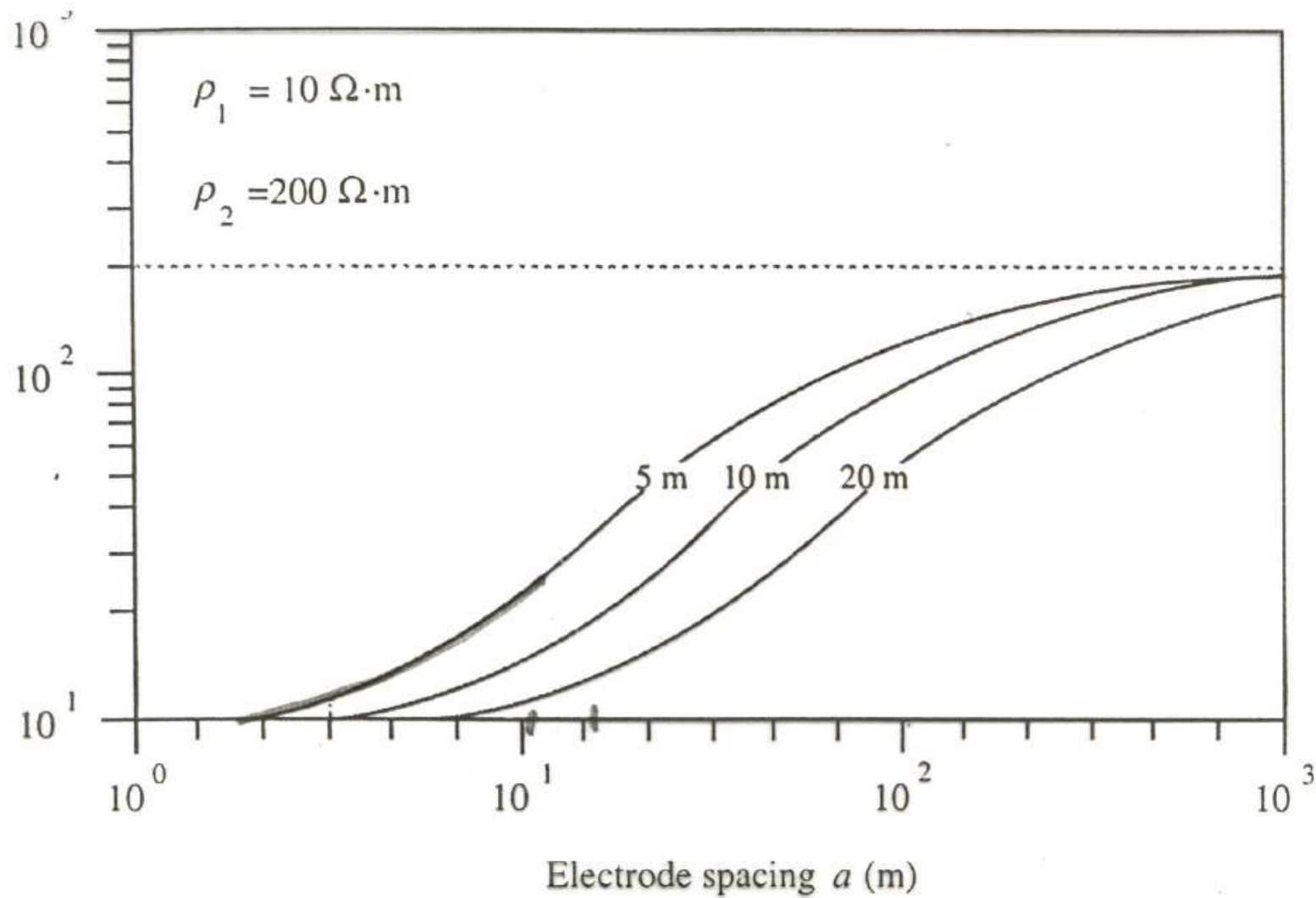
VES: 1 & 2 Layers



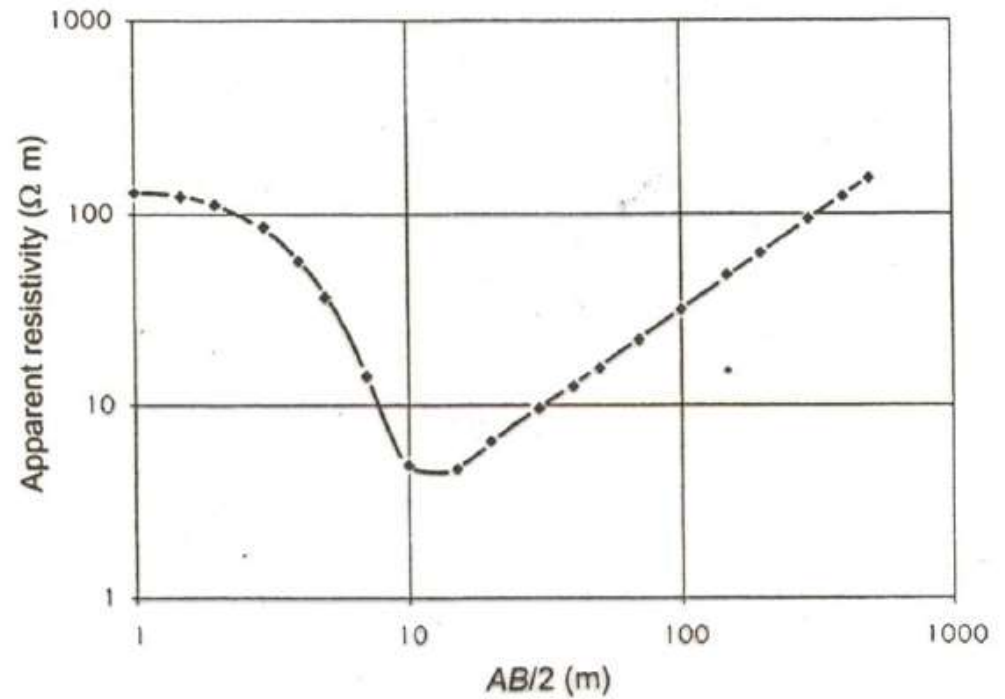
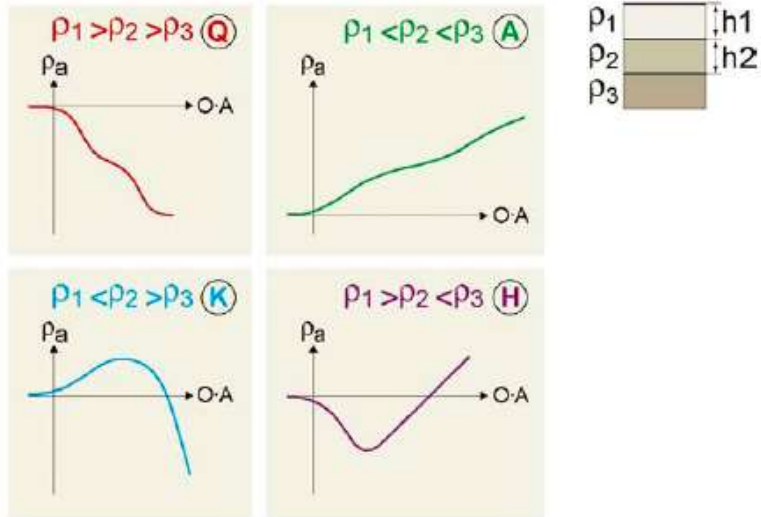
VES: 2 Layers



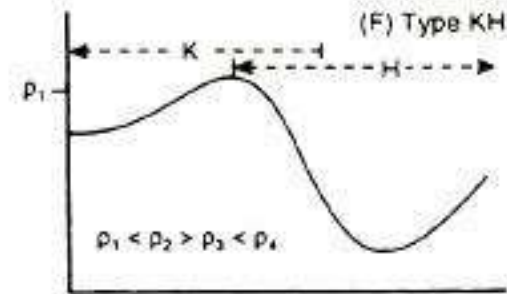
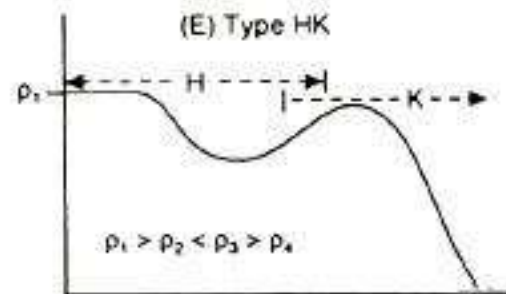
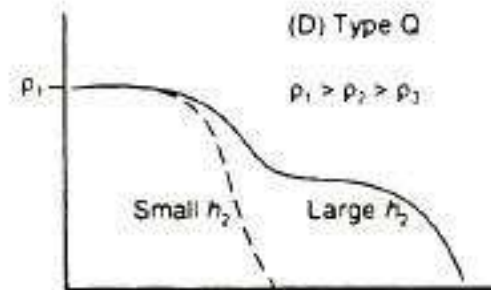
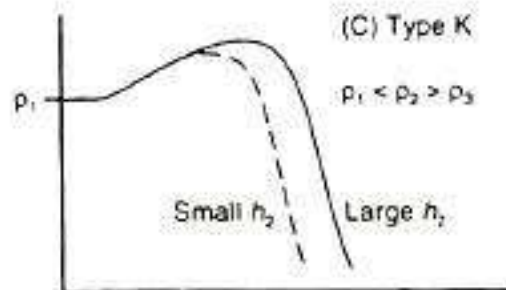
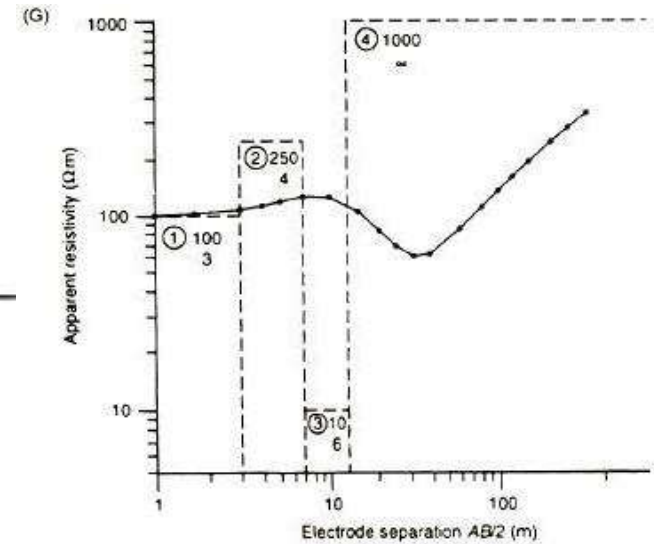
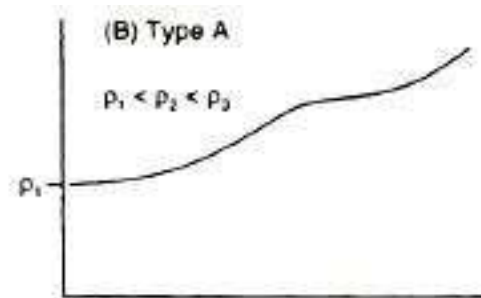
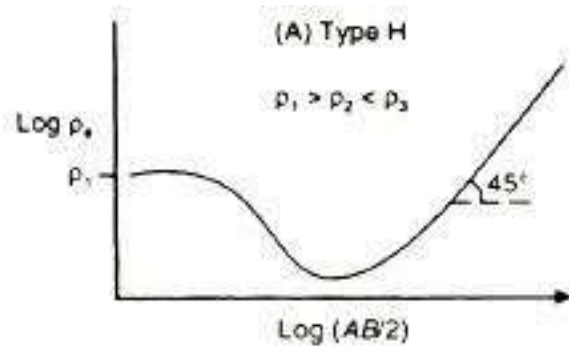
VES: 2 Layers



VES: 3 Layers



VES: 3 Layers



Sounding Curves Remain the Same on Log-Log

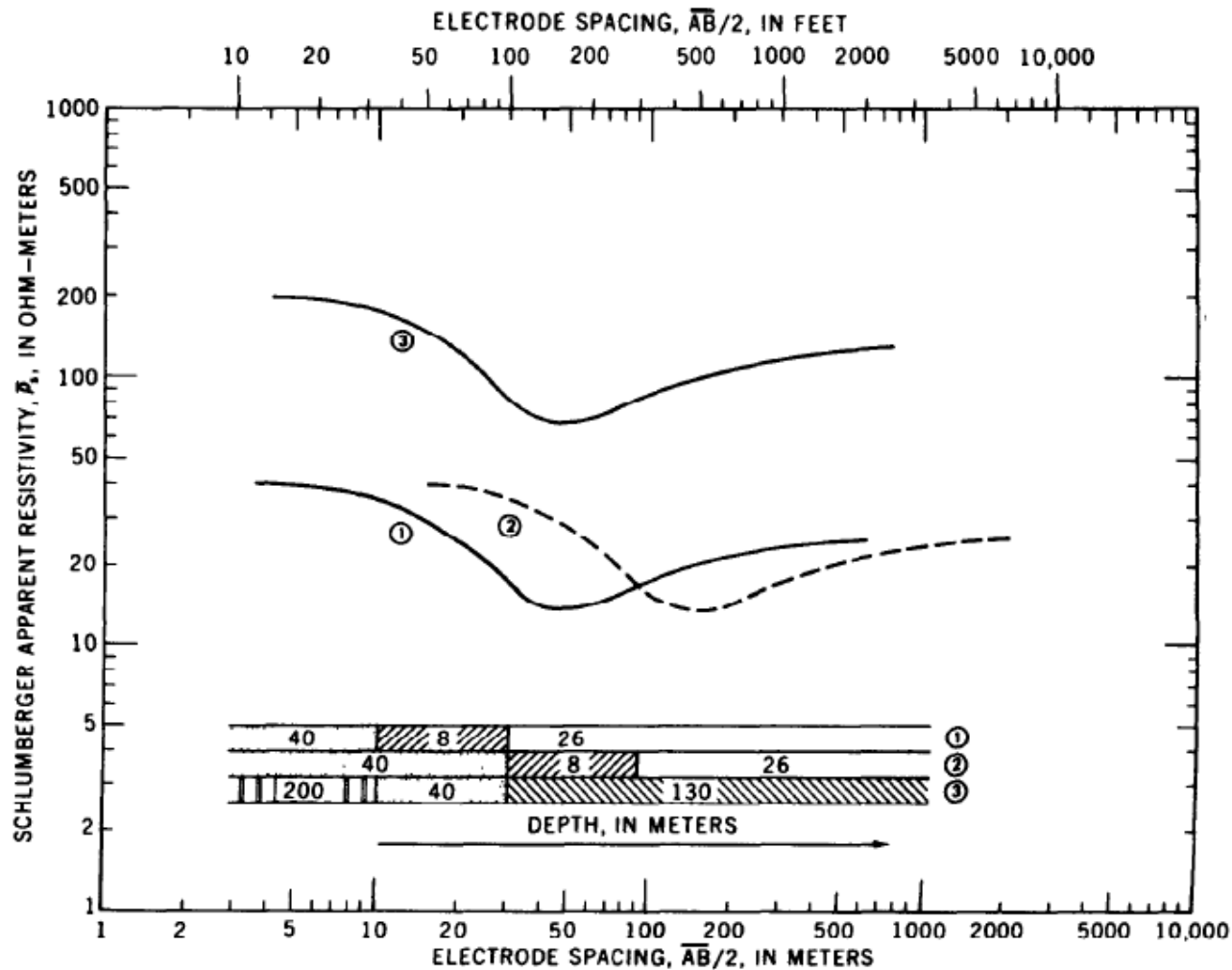


Figure 13.—Logarithmic plot of sounding curves. The layers in model 2 are three times as thick as model 1; the layer resistivities in model 3 are five times as large as model 1; however, the shapes of all three curves are identical.

Sounding Curves Are Different on Normal Plots!

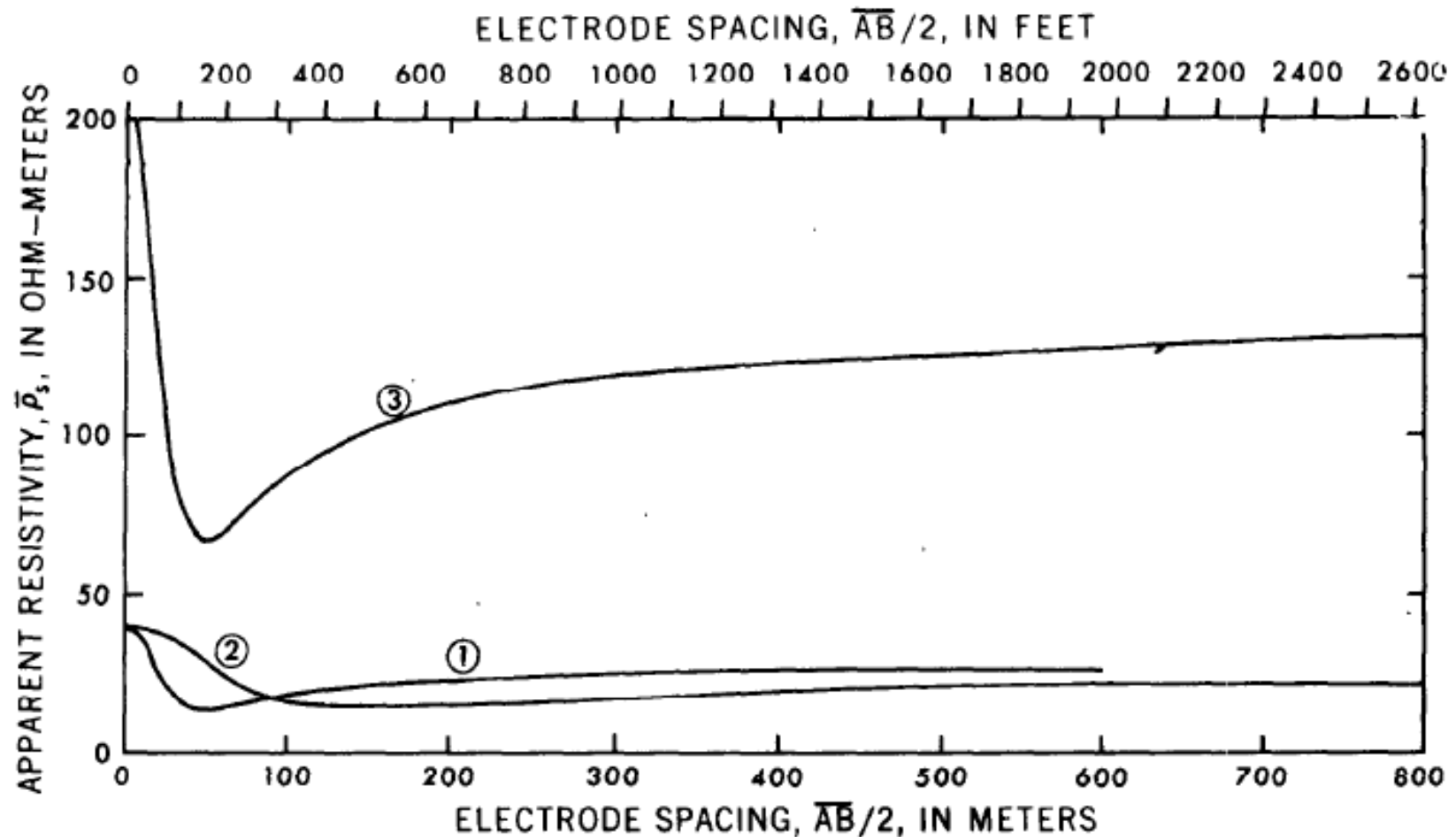


Figure 14.—Linear plot of sounding curves. Earth models are the same as in figure 13. Curve form is not preserved.

Schlumberger Sounding Curves – 3 Layer Earth

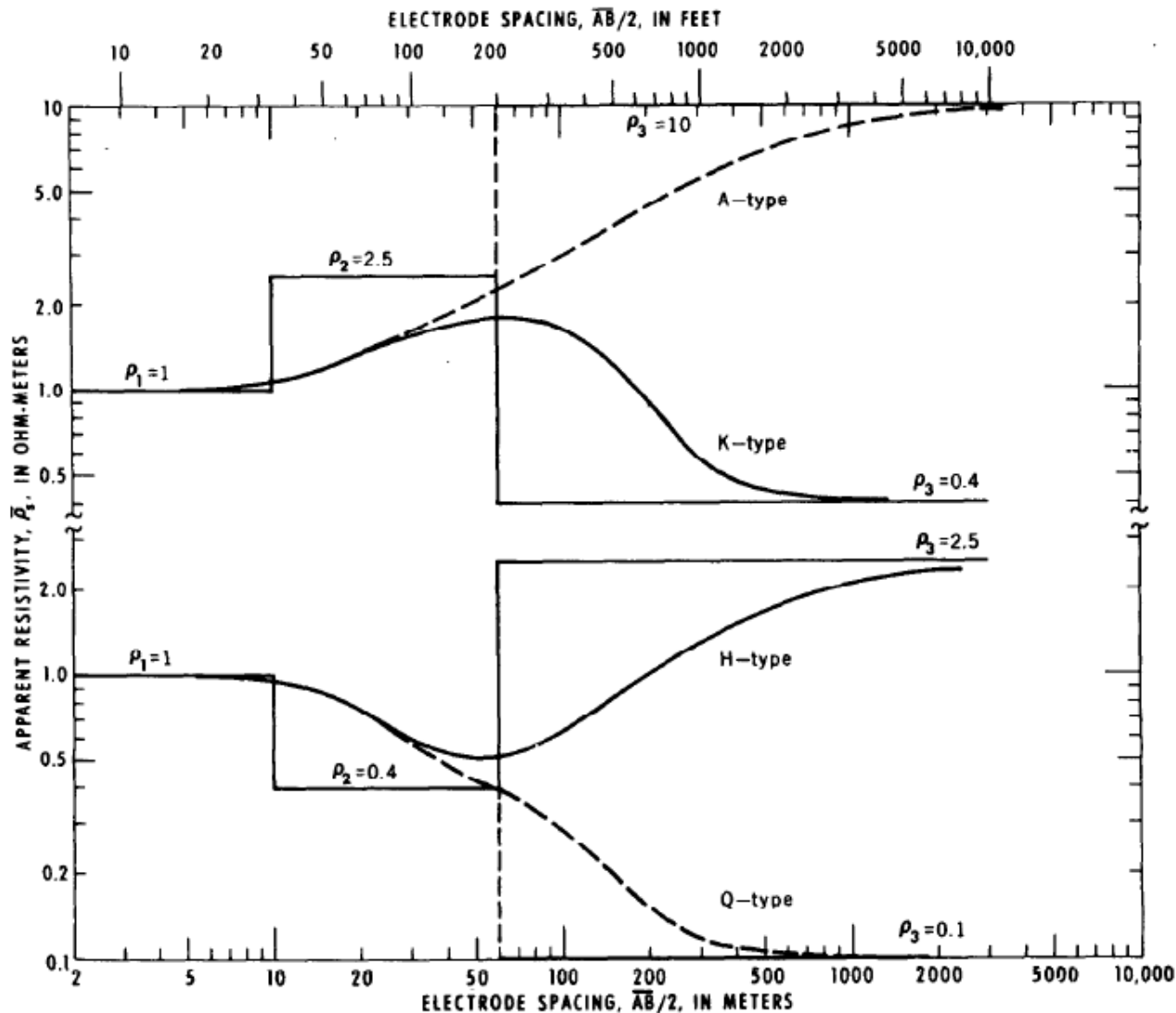


Figure 18.—Examples of the four types of three-layer Schlumberger sounding curves for three-layer Earth models.

Source: USGS Techniques of Water Resources Investigations – D1 Application of Surface Geophysics to Ground-water Investigations

Schlumberger Sounding Curves – 4 Layer Earth

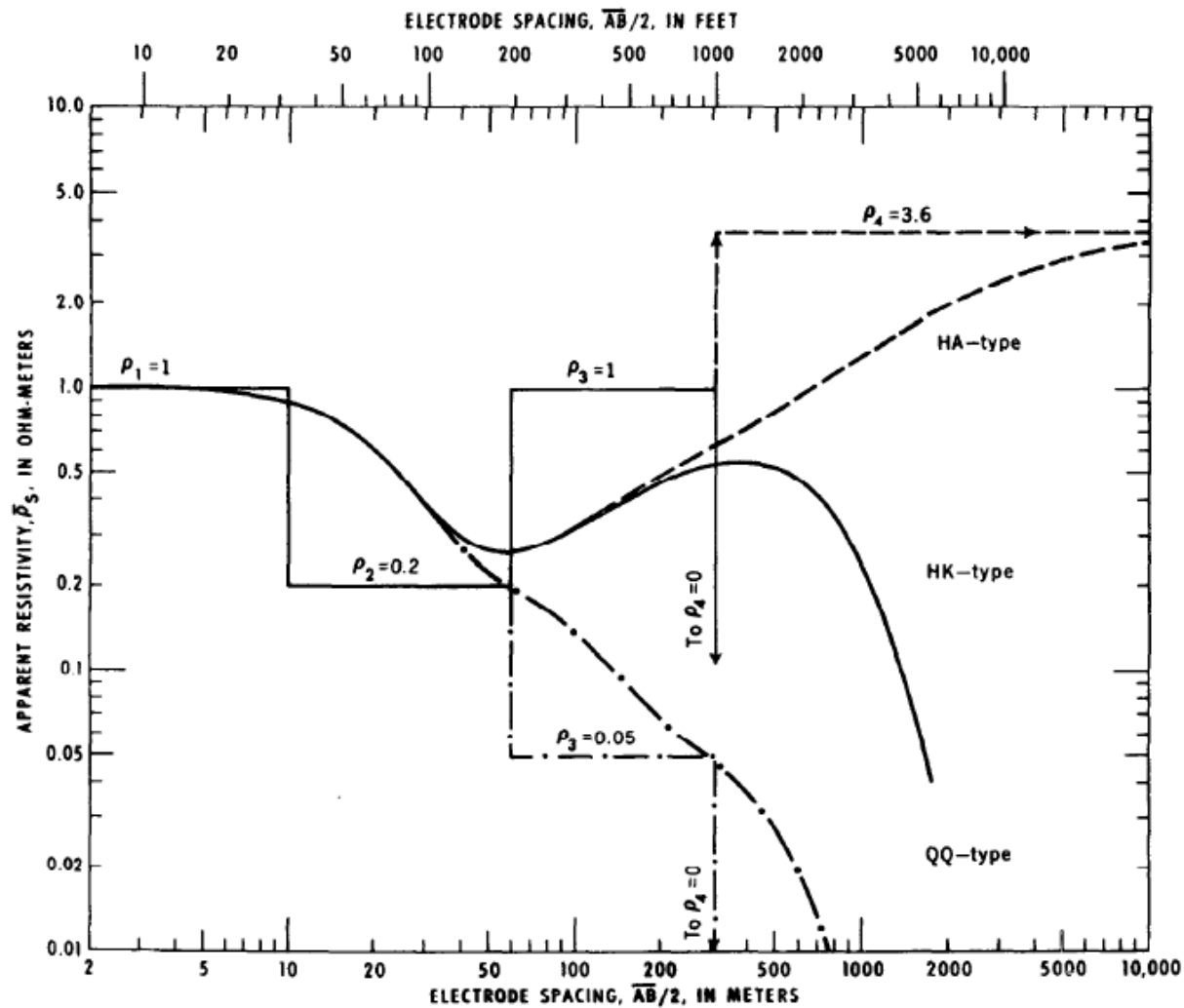
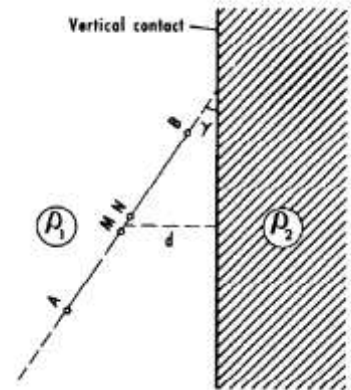
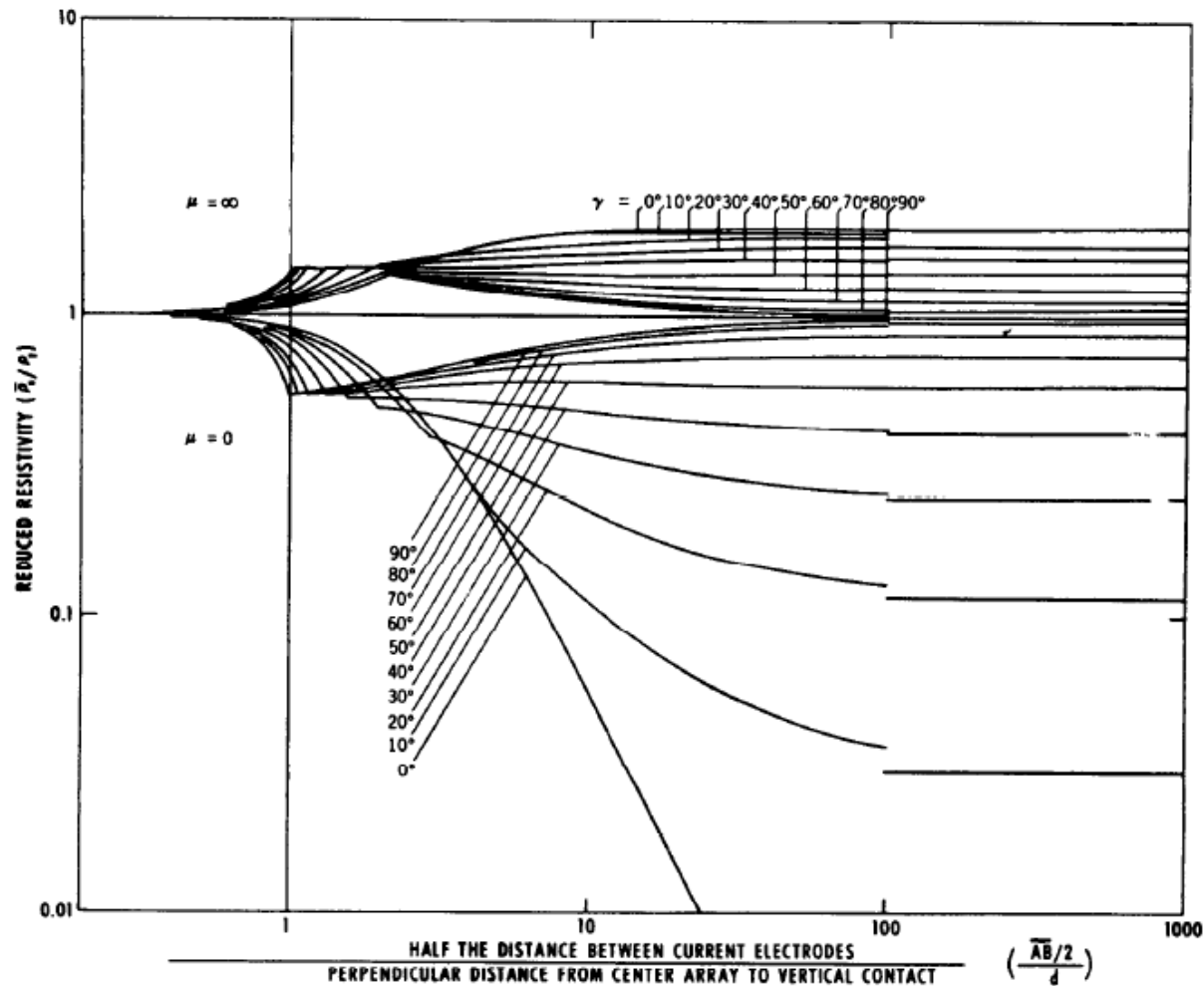


Figure 19.—Examples of three of the eight possible types of Schlumberger sounding curves for four-layer Earth models.

Source: USGS Techniques of Water Resources Investigations – D1 Application of Surface Geophysics to Ground-water Investigations

Schlumberger Sounding Curves – Vertical Contact



Cusp in Sounding Curves

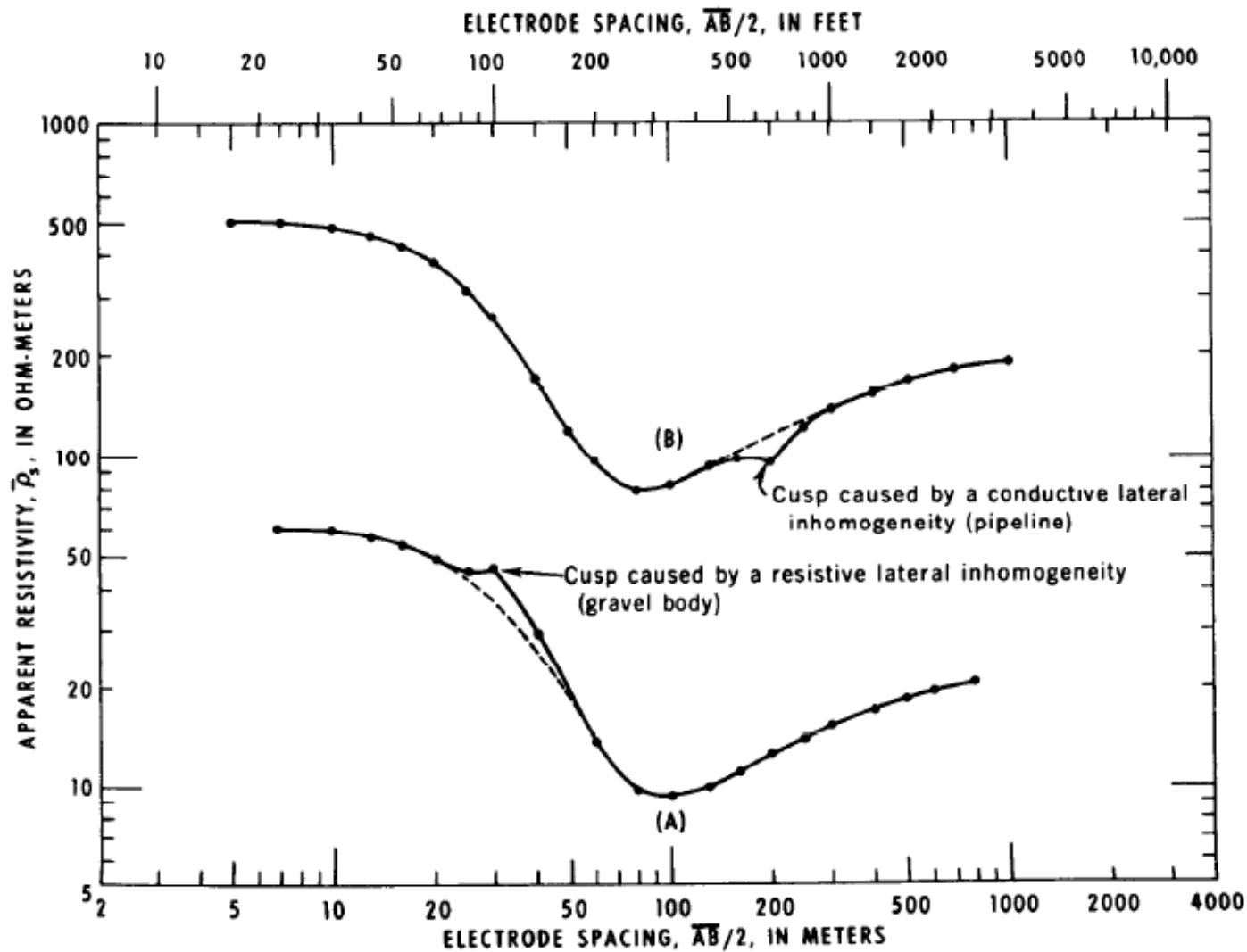


Figure 29.—Distortion of sounding curves by cusps caused by lateral inhomogeneities.

Source: USGS Techniques of Water Resources Investigations – D1 Application of Surface Geophysics to Ground-water Investigations

Sounding Curves Distortion

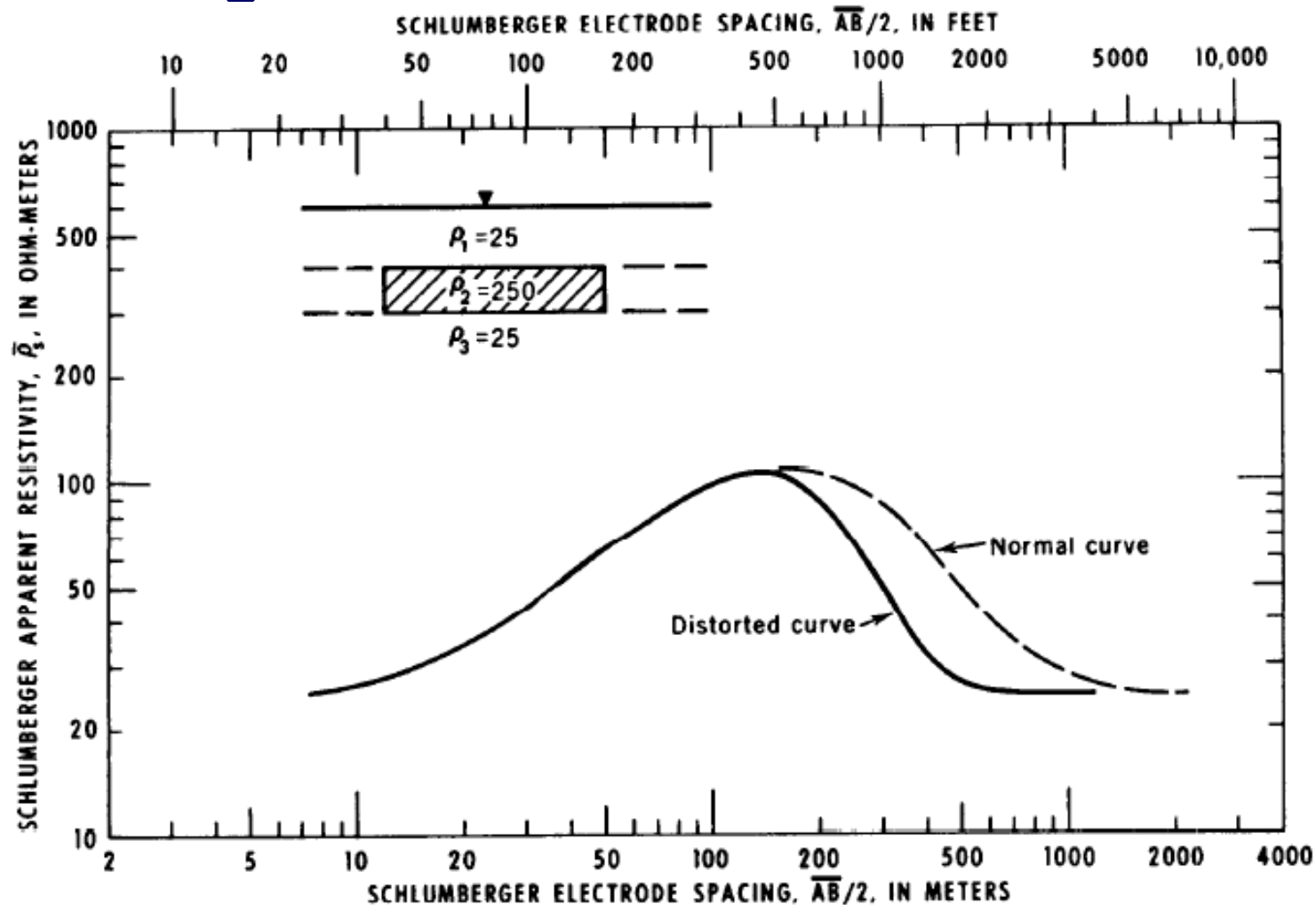


Figure 30.—Example of a narrow peak on a K-type curve, caused by the limited lateral extent of a resistive middle layer (after Alfano, 1959). Reproduced with permission of "Geophysical Prospecting."

Correcting Distorted Sounding Curves

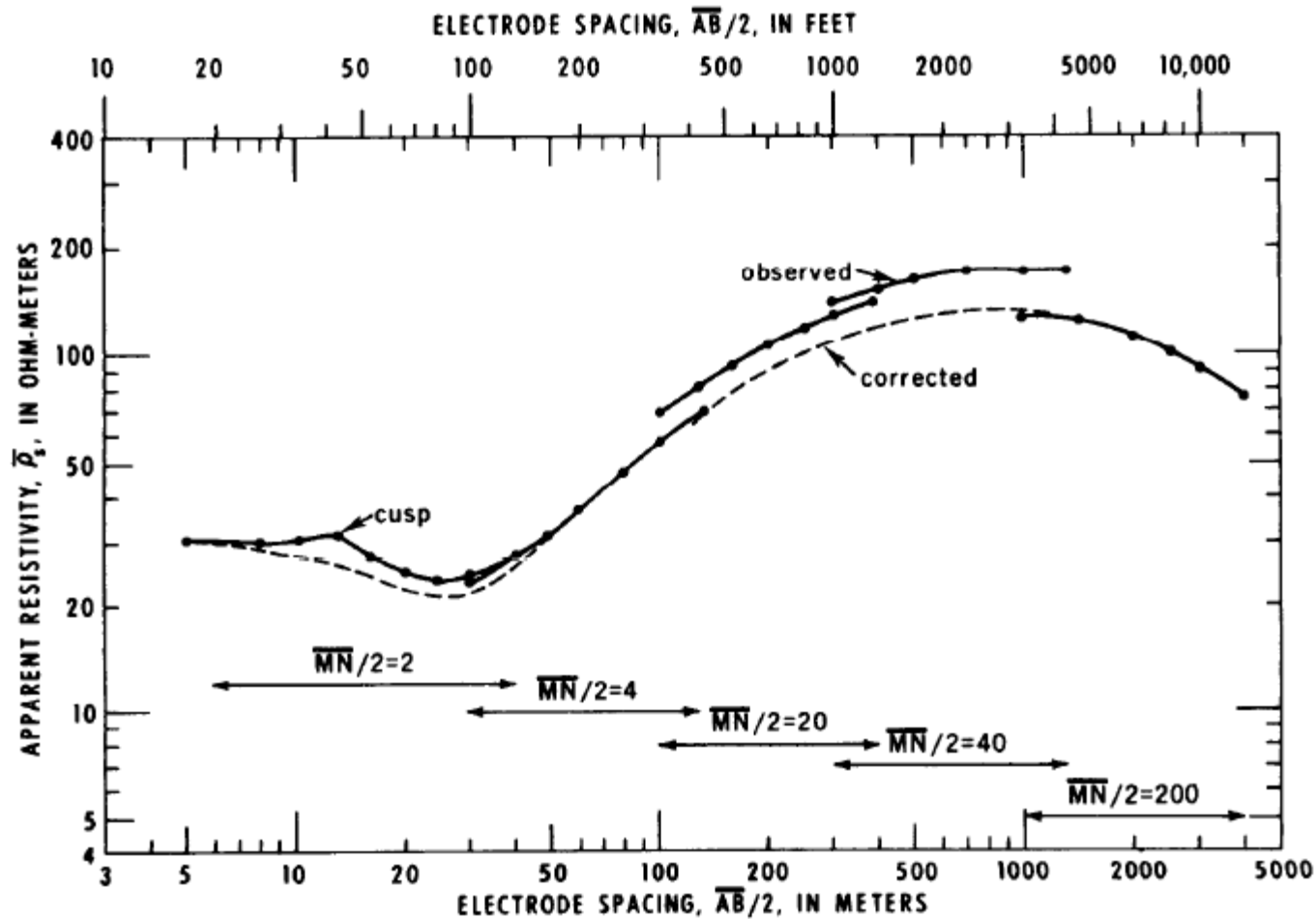


Figure 31.—Example of a distorted HK-Schlumberger curve and the method of correction.

Sounding Curves Distortion

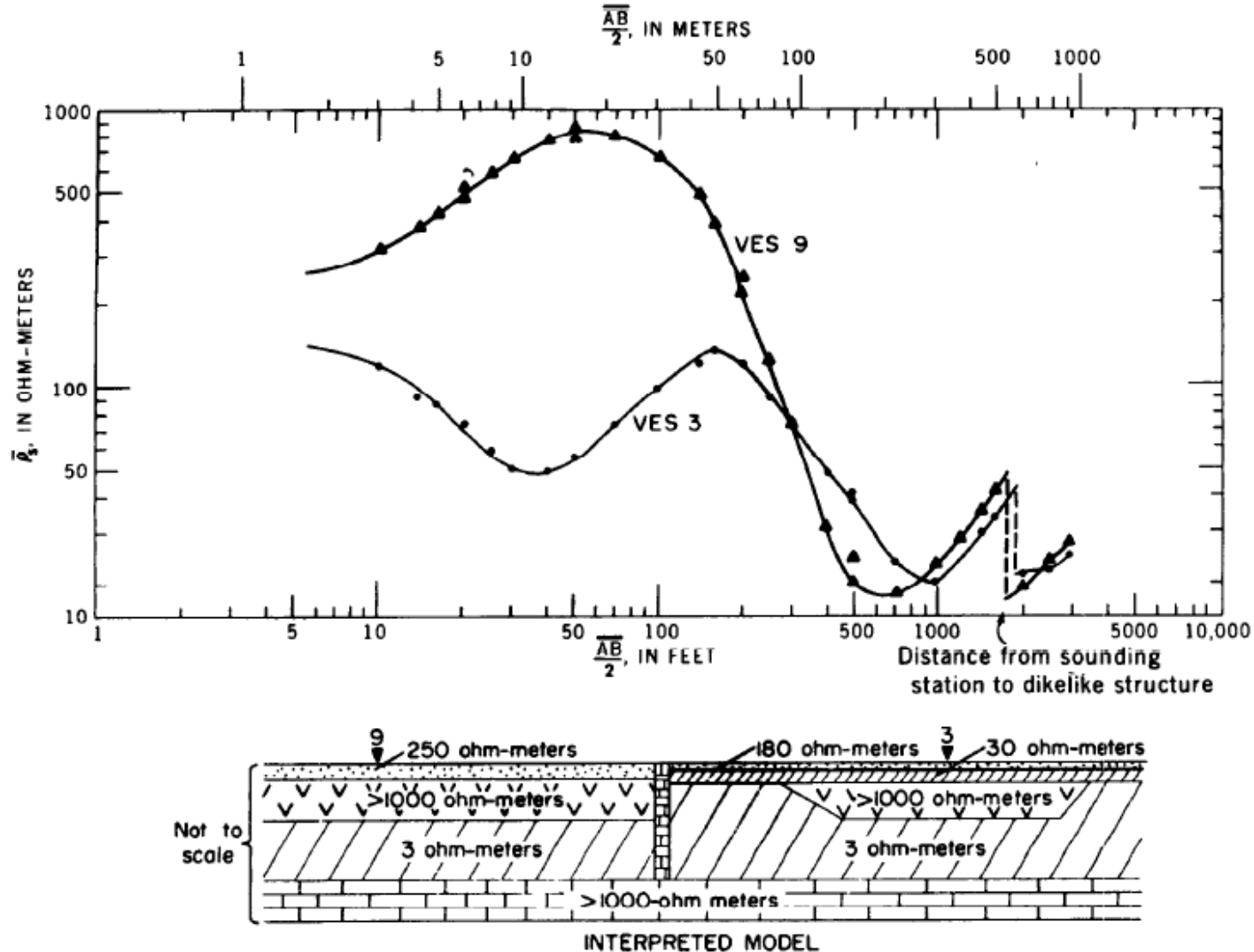


Figure 32.—Examples of tares (discontinuities) on Schlumberger curves caused by a near vertical dike-like structure. (after Zohdy, 1969a). Reproduced with permission of "Geophysics."

Source: USGS Techniques of Water Resources Investigations – D1 Application of Surface Geophysics to Ground-water Investigations

Principle of Equivalence

Transverse Resistance

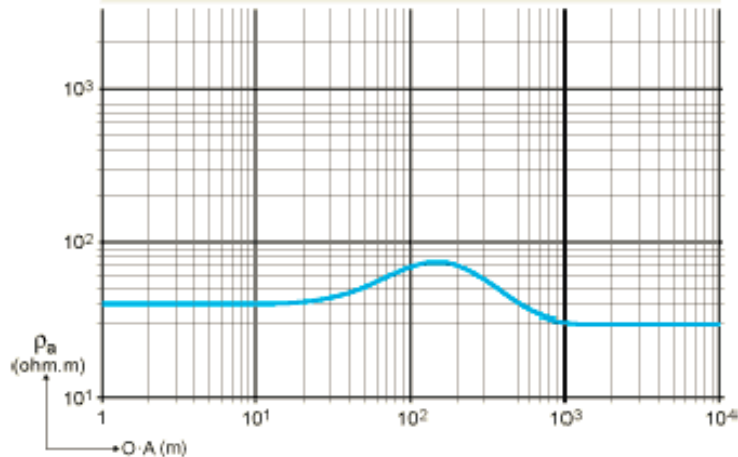
EQUIVALENCE TYPE K ($\rho_1 < \rho_2 > \rho_3$)

INTERPRETATION (A)

Resistivity (ohm.m)	Thickness (m)	Depth (m)
40	36	0
800	10	36
30		46

INTERPRETATION (B)

Resistivity (ohm.m)	Thickness (m)	Depth (m)
40	36	0
400	20	36
30		56



$$R = h\rho$$

Longitudinal Conductance

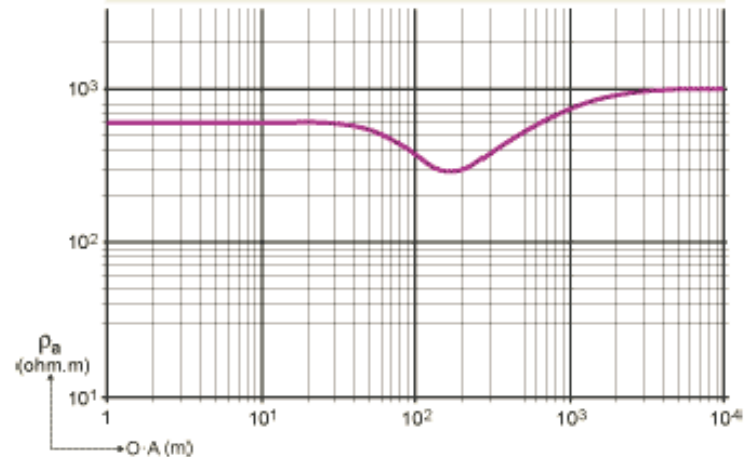
EQUIVALENCE TYPE H ($\rho_1 > \rho_2 < \rho_3$)

INTERPRETATION (A)

Resistivity (ohm.m)	Thickness (m)	Depth (m)
600	50	0
20	10	50
1000		60

INTERPRETATION (B)

Resistivity (ohm.m)	Thickness (m)	Depth (m)
600	50	0
40	20	50
1000		70



$$R = \frac{h}{\rho}$$

Principle of Suppression

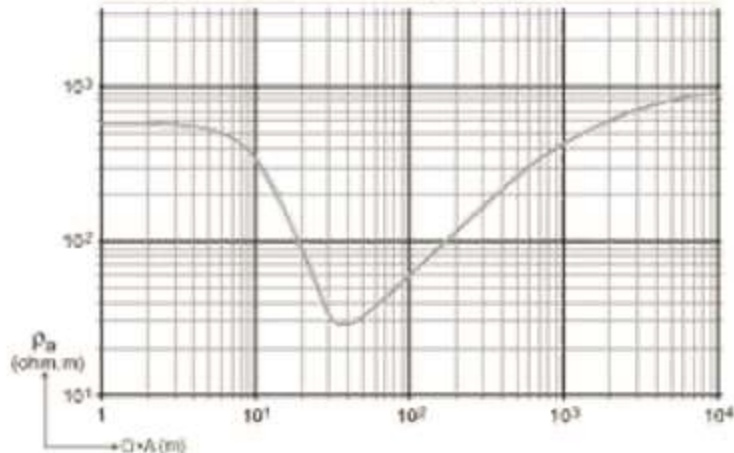
SUPPRESSION TYPE H and A

INTERPRETATION (A)

Resistivity (ohm.m)	Thickness (m)	Depth (m)	
600	6	0	Sandy alterite
20	30	6	Argillous alterite
1000		36	Bedrock

INTERPRETATION (B)

Resistivity (ohm.m)	Thickness (m)	Depth (m)	
600	6	0	Sandy alterite
20	26	6	Argillous alterite
200	3	32	altered bedrock
1000		35	Bedrock



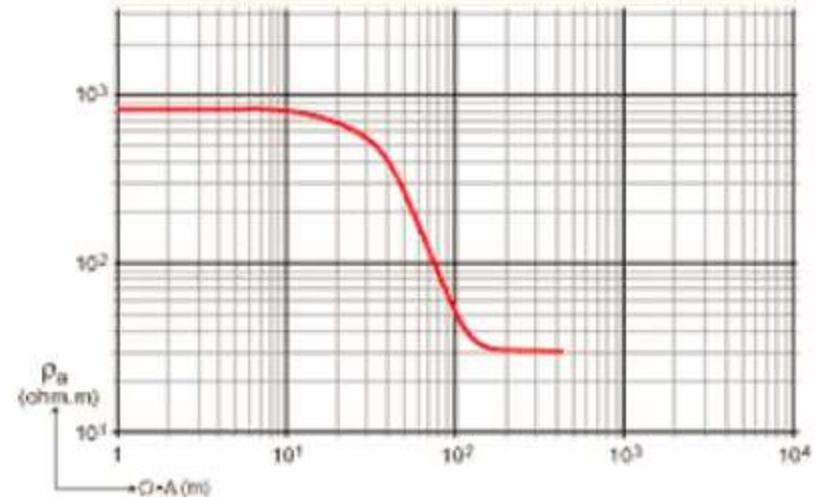
SUPPRESSION TYPE Q ($\rho_3 < \rho_2 < \rho_1$)

INTERPRETATION (A)

Resistivity (ohm.m)	Thickness (m)	Depth (m)
800	21	0
30		21

INTERPRETATION (B)

Resistivity (ohm.m)	Thickness (m)	Depth (m)
800	20	0
200	5	20
30		25



Calibration Sounding

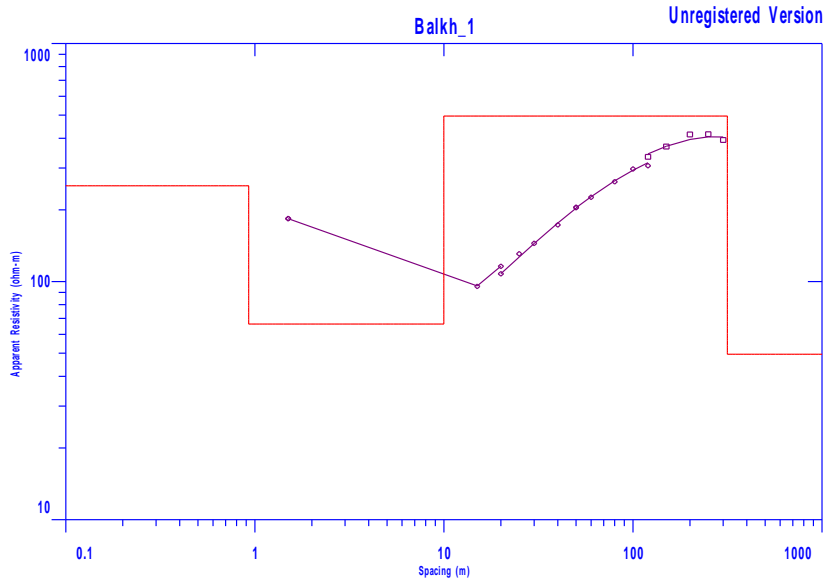
Calibration soundings are carried out to determine the precise resistivity of a formation.

This reduces the problem of equivalence.

VES near a borehole with downhole geophysical logs or on an outcrop.

ALWAYS DO AT LEAST ONE CALIBRATION SOUNDING!

Practical – 1D Inversion Software



Client : Irrigation Department
Project : Balkh
District :
Date : 2013
Field Operator : Ahmad Javid
Interpreted by : A&J

Community : Balkh
Sounding Number : S-01
Coordinates East : E XX.XXXXX
Coordinates North : N XX.XXXXX
GPS Datum : WGS84
Azimuth : XX

Geoelectrical Model RMS Error : 14

Layer Number	1	2	3	4	5	6	7	8
Resistivity (Ohm-m)	258	60	540	10				
Thickness (m)	3.0	9.0	220.8					
Depth (m)	3.0	12.0	232.8					

